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ELECTRICAL DOUBLE LAYER STRUCTURE IN THE PRESENCE OF ADSORBED ORGANIC MOLECULES

by

David Edward Broadhead

A Dissertation Submitted to the Graduate Faculty in Partial Fulfillment of The Requirements for the Degree of DOCTOR OF PHILOSOPHY

Major Subject: Physical Chemistry

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TABLE OF CONTENTS

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	Page
INTRODUCTION	1
THEORY	3
EXPERIMENTAL	9
Materials	9
Apparatus	12
Procedure	16
Problems	18
ANALYSIS OF RESULTS	20
Computer Programs	20
Method of Analysis	21
Accuracy of Electrocapillary Curves	24
Accuracy of Results	27
Results	30
INTERPRETATION OF RESULTS	33
SUMMARY	40
SUGGESTED MODIFICATIONS AND EXTENSIONS	42
BIBLIOGRAPHY	44
ACKNOWLEDGEMENTS	47
APPENDIX A	48
Figures Cited in Text	48
APPENDIX B	93
Computer Program Listings	93

	Page
APPENDIX C	117
Output Data From Computer Programs	117
APPENDIX D	131
Tables Cited in Text	131

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INTRODUCTION

At every interface between two immiscible phases, there exists an array of charged particles and oriented molecules called the electrical double layer. In the case of the metalsolution interface this double layer consists of a layer of electrons (or holes) in the metal, a layer of adsorbed ions and molecules, and a diffuse layer of ions extending out into the bulk solution.

If a potential difference is applied between the metal and the solution, a current may flow across the interface. It is possible, however, that a range of potentials exists for which no charge is transferred across the interface, causing it to act as a capacitor. A system of this second type is called an ideal polarized electrode, and while it can never be fully realized experimentally, close approximations to it are attainable. The study of electrodes which behave as ideal polarized electrodes is known as electrocapillarity.

Historically, mercury has been the metal chosen most frequently in electrocapillary studies. There is a range of about 1.5 volts between potentials respectively at which hydrogen or oxygen evolution reactions lead to appreciable current flows. Since it is a liquid, its surface can be easily cleaned, it is free from mechanical strains, and its interfacial tension is easily measured.

The study of electrocapillarity began with Lippmann

(1) in 1875, who was the first to realize that a measurement of interfacial tension at the mercury-solution interface is meaningless unless the potential difference across the interface is known. Of the early workers, Gouy is the most widely known, due to his extensive cataloging of electrocapillary data for many systems (2-4), and his formulation of a theory of the electrical double layer (5, 6). An excellent review of the earlier work (up to 1947) in electrocapillarity, which is also a good introduction to the subject, was published by Grahame (7).

Since many reviews have been published recently on the subject of the electrical double layer (8-12), no attempt will be made here to summarize the more recent work in this field.

THEORY

The basic thermodynamic relation between the variables at an electrified interface is the Gibbs adsorption equation

$$-d\gamma = QdV + SdT + \sum_{i} \Gamma_{i} d\mu_{i}, \qquad (1)$$

where γ is the interfacial tension, Q is the charge density on the metal surface, V is the polarizing potential, S is the surface entropy, T is the absolute temperature, μ_1 is the chemical potential of the ith component of the system, and Γ_1 is the surface excess of the ith component. Since two similar equations can be written for the metal and the solution, respectively, it is possible to eliminate two of the terms on the right-hand side of Equation 1. This is usually done by choosing $\Gamma_{\rm Hg} = \Gamma_{\rm H_2O} = 0$.

Since in this thesis we shall be concerned with the adsorption of neutral organic molecules at the interface, the concentration of the electrolyte used and the temperature will always be the same. Hence the Gibbs equation for this special case reduces to

$$-d\gamma = QdV + \Gamma_{\rm org} d\mu_{\rm org} .$$
 (2)

The interfacial tension now can be seen to be a function of two variables, the potential difference applied across the interface and the chemical potential of the organic substance present in the solution. Experimental data are usually obtained by finding the interfacial tension as a function of

potential at constant concentration of the organic solute. A plot of the data obtained in this manner, which is roughly parabolic in shape, is called an electrocapillary curve.

Several useful thermodynamic relations are obtainable from Equation 2. The charge density is found from the first derivative of the electrocapillary curve, since

$$Q = - \left(\frac{\partial \gamma}{\partial V}\right)_{\mu_{\text{org}}} .$$
 (3)

It can be seen from Equation 3 that the maximum interfacial tension occurs when the charge on the mercury is zero. Since the differential capacitance, C, is the derivative of charge with respect to potential,

$$C = - \left(\frac{\partial^2 \gamma}{\partial V^2}\right)_{\mu_{\text{org}}}, \qquad (4)$$

and the capacity of the electrical double layer can be obtained from the second derivative of the electrocapillary curve.

The surface excess of the organic adsorbate is given by

$$\Gamma_{\rm org} = - \left(\frac{\partial \gamma}{\partial \mu_{\rm org}}\right)_{\rm V} . \tag{5}$$

It can be seen that if $\Gamma_{org} > 0$, the addition of an organic substance to the solution causes a lowering of the surface tension. Experimentally this lowering is more pronounced near the electrocapillary maximum, i.e., in the region of low charge density. This is because the organic

solute, which is usually less polar than the solvent, is displaced from the surface at high charge densities by the water and ionic species present.

In practice it is convenient for calculations to use the surface pressure, π , defined by $\pi = \gamma_0 - \gamma$, where γ_0 is the interfacial tension obtained with no organic material present in the solution. Equation 5 then becomes

$$\Gamma_{\rm org} = \frac{1}{RT} \left(\frac{\partial \pi}{\partial \ln a} \right)_{\rm V} , \qquad (6)$$

where a is the activity of the organic solute in the bulk solution. The activity used for the solutes in this thesis is referred to pure liquid solute as standard state and is approximated by the reduced concentration (concentration divided by saturation concentration).

In order to describe the dependence of the amount of organic solute adsorbed on the bulk activity at a given potential, the Frumkin isotherm (13) has been used. The equation for this isotherm is

$$\frac{\theta}{1-\theta} = B_0 a e^{2\alpha\theta} , \qquad (7)$$

where $\theta = \Gamma/\Gamma_m$ is the fractional surface coverage (Γ_m being the surface excess of the adsorbate at monolayer coverage), B_0 is a constant reflecting the interaction of the adsorbate with the mercury surface, and α is a constant reflecting the interactions between molecules of the adsorbate. This equation is based on the regular localized monolayer model, with random distribution of adsorbed molecules in the monolayer.

Two useful standard free energies of adsorption may be obtained from the Frumkin isotherm as follows. Equilibrium between molecules in the solution and on the surface implies

$$\mu_{\rm b} = \mu_{\rm s} , \qquad (8)$$

where μ_b and μ_s are the chemical potentials of the molecules in the bulk solution and on the surface, respectively. In the solution

$$\mu_{\rm b} = \mu_{\rm b}^{\rm O} + RT \ln a, \qquad (9)$$

and on the surface

$$\mu_{\rm s} = \mu_{\rm s}^{\rm O} + RT \ln \gamma_{\rm s} \frac{\theta}{1-\theta} , \qquad (10)$$

where $\gamma_{\rm g}$ is the surface activity coefficient.

Substituting Equation 7 into Equation 9 gives

$$\mu_b = \mu_b^o - RT \ln B_o + RT \ln\{e^{-2\alpha\theta}(\frac{\theta}{1-\theta})\} .$$
 (11)

Therefore, Equation 8, together with Equations 10 and 11 implies that

$$\mu_{\rm S}^{\rm o} - \mu_{\rm b}^{\rm o} = -RT \ln B_{\rm o}$$
 (12)

1. f

$$Y_{\rm s} = e^{-2\alpha\theta} . \tag{13}$$

The standard state for the adsorbate on the surface implied by Equation 13 satisfies $\lim_{\theta \to 0} \gamma_s = 1$, and physically reflects a state in which an adsorbate molecule has no other adsorbate molecules as near neighbors. Hereafter this will be referred to as an infinite dilution-based standard state. The free energy given by Equation 12 is therefore not very easily interpreted, as it refers to standard states based on pure solute in the solution and infinite dilution on the surface.

The interaction free energy per mole at $\theta = 1$ is given by

$$RT \ln \gamma_{2} = -2\alpha RT . \qquad (14)$$

Hence

$$\Delta G_1^0 = -RT \ln B_0 - 2\alpha RT, \qquad (15)$$

where ΔG_1^0 is the standard free energy of adsorption referred to standard states based on pure adsorbate both in solution and on the surface.

Similarly, the free energy required to transfer one mole of adsorbate from an infinite dilution-based state in the bulk solution to pure solute is -RT ln f_0 , where f_0 is the activity coefficient of the adsorbate at an infinite dilution-based state, referred to pure solute as standard state. Therefore

$$\Delta G_{\Omega}^{O} = -RT \ln B_{\Omega} - RT \ln f_{\Omega}, \qquad (16)$$

where ΔG_0^0 is the standard free energy of adsorption referred to standard states based on infinite dilution of adsorbate both in solution and on the surface.

The free energies given in Equations 15 and 16 have been determined for a number of different adsorbates (14), and a correlation between the free energy of adsorption and the polarizability of the molecule will be established in a later section.

EXPERIMENTAL

Materials

Mercury

Mercury was used as received from Bethlehem Apparatus Co. It was triply distilled under vacuum, and had an evaporation residue of one part in ten million.

Water

All water used in preparing solutions and as the final rinse in the cleaning of glassware was quadruply distilled. Tap distilled water was redistilled from alkaline permanganate solution in a Barnsted still. This water was distilled again through a fused silica continuous double distillation column.

Perchloric acid

Perchloric acid was used as the electrolyte so that results obtained could be more readily compared with those of previous workers in this laboratory. Baker Analyzed Reagent perchloric acid was used without further purification.

The purification of the mercury, water, and perchloric acid was judged to be sufficient by the reproducibility and precision of the electrocapillary curves obtained with no organic adsorbate present. If even a minute amount of a surface active substance had been present in any of these materials, the interfacial tensions would not have remained constant over the time required for a measurement (1 to 5 minutes).

Adsorbates

All organic compounds used were purified by distillation in a Nester/Faust spinning band column. A reflux ratio of 20:2 was maintained during take-off and only the middle onethird of the product was retained. The boiling point of the product was always constant to within 0.3° C. For cyclohexanol and cyclohexanone a vacuum distillation was performed, due to their high boiling points. The pressure in each case was maintained at 70 ± 1 mm of Hg by a pressure regulator, also manufactured by Nester/Faust.

Preparation of solutions

All glassware which came into contact with the solutions or their components was cleaned with alcoholic sodium hydroxide, followed by a solution of potassium dichromate in sulfuric acid, then rinsed several times with tap distilled water and finally with quadruply-distilled water.

The perchloric acid solutions were prepared by first diluting the stock solution to make a large volume of one normal acid, from which the tenth normal solutions were prepared by further dilution. All tenth normal solutions were titrated to the phenolphthalein end point with standard 0.1000N sodium hydroxide. No solution was used which deviated by more than 0.0005N from the desired concentration.

Solutions of 3-pentanol and chloroform were prepared by delivering a measured volume of the liquid with a micropipette

into a volumetric flask, and diluting to volume with O.1N perchloric acid. Cyclohexanol and cyclohexanone solutions were prepared by dilution of the saturated solution with O.1N perchloric acid.

Solubilities

The solubility of 3-pentanol in 0.1N perchloric acid was determined by preparing several solutions of known concentration, and determining the refractive index and density of these solutions and of the saturated solution. Each of these quantities, when plotted against concentration, yielded a straight line which on extrapolation gave a solubility of $0.588 \pm 0.005M$.

The solubility of chloroform could not be determined by the above method due to the difficulty of dissolving the chloroform when the solutions were near saturation. Instead, standard solutions were prepared of chloroform in heptane which had been previously saturated with 0.1N perchloric acid. The absorbance of these solutions at 230 Å was measured and plotted against concentration. The chloroform in a saturated (0.1N perchloric acid) solution was then extracted with several known volumes of heptane (previously saturated with 0.1N perchloric acid) and the absorbance of the resulting solution measured. An interpolation of the absorbance plot showed the solubility of chloroform to be 0.0494 + 0.0005M.

The solubility of cyclohexanol was determined by adding known volumes of 0.1N perchloric acid to a known volume of cyclohexanol until the small bubbles of the organic phase disappeared. Cyclohexanol was then added dropwise until the bubbles remained after vigorous shaking. The average of these results was taken as the solubility, $0.217 \pm 0.005M$.

The solubility of cyclohexanone was determined from electrocapillary measurements. The technique used will be described in a later section.

Apparatus

The use of the capillary electrometer in obtaining interfacial tension data at the mercury-solution interface began with Lippmann (1) in 1875. All modern electrometers are merely refinements of his basic apparatus. A conical capillary containing mercury is placed in a solution, the interface between the two liquids being formed in the capillary. Methods of varying the pressure at the interface and of applying a potential across the interface must be devised. The interfacial tension, γ , is then determined by

$$\gamma = \frac{R\Delta P}{2\cos \alpha} \tag{17}$$

where R is the radius of the capillary, ΔP the pressure difference across the interface, and $_{A}$ the contact angle between the mercury and the solution, which is assumed to

be zero. If measurements are made with the interface always in the same position, R is a constant. When the interfacial tension is varied by changing the polarizing potential, the pressure ΔP is then adjusted so as to return the interface to its original position.

In order to obtain the radius of the capillary at this reference position, the electrocapillary curve of a standard solution was determined. The maximum interfacial tension of the standard solution being known independently, the radius of the capillary could then be calculated. The solution originally used as a standard was 0.05M sodium sulfate, for which the maximum interfacial tension had been determined by sessile drop measurements (15) as 426.2 ± 0.2 dynes/cm at 25.0 + 0.3 degrees Centigrade. After several electrocapillary curves of both 0.05M sodium sulfate and 0.1N perchloric. acid had been taken with the same capillary, it was decided to use 0.1N perchloric acid as a standard, since the data obtained with this solution were more reproducible. The interfacial tension of 0.1N perchloric acid at the electrocapillary maximum was taken as 425.6 dynes/cm at 25.0 ± 0.1 degrees Centigrade.

The capillary electrometer and its associated pressure system was designed by Gordon Potter and is shown schematically in Figure 1. The capillaries were formed from precision bore Pyrex capillary tubing of internal diameter 0.0008 inches by drawing out the tubing in a gas flame until a

tenfold reduction in the outside diameter was attained. The mercury reservoir above the capillary was about 23 cm high, the diameter at the top being much larger in order to minimize the change in height caused by expelling mercury during the experiment.

A tungsten wire was sealed through the glass near the top of the mercury reservoir to provide an electrical connection with the mercury side of the interface. The reference electrode, a Beckman fiber junction saturated calomel electrode, was placed in the solution at the opposite end of the cell from the capillary. A Leeds and Northrup K-3 potentiometer was used to control the potential supplied by four mercury cells. The drift in the potential of these cells after they had been in the circuit for several hours was negligible, so that the potentiometer needed to be calibrated only at 5-10 minute intervals to maintain one millivolt accuracy. Calibration was done with an Eppley standard cell, using a Leeds and Northrup D-C Null Detector, model 9834.

The pressure at the interface was varied by applying pressure to the gas above the mercury with a bellows system. Four 100 cc glass syringes, mounted in a screw-driven press, were used for coarse adjustment, and fine adjustment was achieved with a single 30 cc syringe mounted in a separate press. All syringes were lubricated with stopcock grease to prevent leakage of gas around the edges. A Texas Instruments,

Inc. Fused Quartz Precision Pressure Gauge was used to measure the gas pressure, rather than a mercury manometer, as had been previously employed. The use of this instrument was responsible for the greatly improved precision of the electrocapillary data. The precision of the gauge was an order of magnitude greater than the best precision obtained for the electrocapillary data. Since measurements took only a matter of seconds, the interfacial tension could be measured immediately following expulsion of a mercury drop and before a significant amount of impurities could diffuse to the interface.

In order to always return the interface to the same position a Unitron stereomicroscope was used to view the capillary, a high intensity lamp being directed through the length of the cell for illumination. A reticular scale within the eyepiece enabled the position of the interface to be determined with respect to the hole in the tip of the capillary. Optically plane glass was used for the ends of the cell to eliminate distortion.

The height of the mercury column and of the solution above the tip of the capillary were measured with a Gaertner cathetometer to a precision of 0.02 mm. Vibrations were reduced by resting the cathetometer on a concrete block stand and by attaching the capillary electrometer to a Dexangle frame which rested on a heavy piece of soapstone.

Temperature control was achieved by the use of a steamreheat air conditioner which maintained the temperature of the air surrounding the electrometer and mercury column at 25 ± 1 degree Centigrade. Water from a large bath thermostated to 25.0 ± 0.1 degrees Centigrade by a Haake temperature controller was circulated through coils in the center of the electrometer.

Procedure

As was noted by Kelsh (16), newly prepared capillaries were found to take up to two weeks after initial wetting to obtain a constant radius. All capillaries were therefore aged by soaking in O.1N perchloric acid solution for at least two weeks before calibration. Since a different capillary was used for each adsorbate studied, it was possible to dismantle and thoroughly clean the electrometer cell before each new set of experiments, thereby removing any traces of the previous adsorbate. After the initial cleaning, the cell was merely rinsed several times with the solution to be added.

After pouring the solution into the cell and installing the calomel electrode, cathetometer readings were taken of the top of the mercury reservoir, the level of the solution in the cell and the bottom of the capillary. These readings were taken only at the beginning and end of each experiment, since the mercury level only dropped by about a tenth of a millimeter during each run.

For the first few electrocapillary curves taken, purified nitrogen was bubbled through the cell prior to the experiment to remove oxygen from the solution. After retaking these curves without first removing the oxygen, it was found that there was no detectable difference in the results, and the procedure was discontinued.

In taking each data point, the potentiometer was first calibrated and the desired potential applied. A drop of mercury was then expelled from the tip of the capillary to provide a fresh surface, presumably free of impurities. The pressure was then adjusted with the bellows to bring the interface to the reference point in the capillary, and the pressure gauge was read. Several oscillations of the interface were made about the reference point by means of the bellows to make sure the mercury was not sticking at this point. Another drop of mercury was expelled and the process repeated as a check. Readings were usually reproducible to within 0.03 dynes/cm.

In order to observe any time-dependent errors in the data, points were taken at even 100 mV intervals proceding from the lowest to the highest potential applied, then the 50 mV points in between were taken in the reverse direction.

Problems

Although interfacial tensions were reproducible to within 0.03 dyne/cm, it was found that the scatter of the points when plotted against potential was more than an order of magnitude larger than this for 3-pentanol. When taking the data it was noticed that the initial value of the interfacial tension was not very reproducible, but if a time varying from three to twenty minutes elapsed after the expulsion of a mercury drop, reproducibility was obtained. At the time the possibility of impurities was not considered, as a gas phase chromatographic analysis had shown that any impurities in the 3-pentanol were less than one-tenth of one percent. On later reflection, however, it was decided that impurities, even in this low a concentration, could have reached the interface in appreciable amounts by ten minutes or so.

When the chloroform data were taken the initial value of the interfacial tension was recorded, assuming that coverage of the surface with chloroform would be as complete as possible within a few seconds due to its relatively high concentration compared to that of any impurities present. Considerable scatter was still obtained in the electrocapillary points for chloroform, but this time the scatter appeared to be timedependent. In order that the reference port of the pressure gauge be at the same pressure as the gas above the solution,

the central port of the electrometer cell had been left loosely stoppered. Enough chloroform had evidently evaporated from the solution to cause a measurable rise in the interfacial tension during the experiment.

A method of correcting the data for evaporation was devised, and will be presented in a later section. To prevent this from being as much of a problem, however, relatively non-volatile solutes were chosen for future work. Much less scatter was observed in the electrocapillary curves for cyclohexanol.

After much deliberation, an absurdly simple solution to the evaporation problem was devised. The reference port of the pressure gauge was simply connected to the central port of the electrometer cell, thus providing a closed system and minimizing evaporation. The data for cyclohexanone were taken using this modified apparatus, and the scatter in the data was greatly reduced.

When solutions of the three lower concentrations of cyclohexanone were run, reproducible initial values for the interfacial tension were not obtainable for potentials negative with respect to the electrocapillary maximum. A gas chromatogram was taken of the cyclohexanone used, and no impurity could be found with a concentration greater than one-tenth of one percent. Due to the method used in analyzing the data, however, useful results were still obtained for this compound.

ANALYSIS OF RESULTS

Computer Programs

Several computer programs were written for use in data analysis. The output from these programs could probably have been obtained more quickly by hand calculation and graphing, since much time was spent in devising, coding, debugging, and revising the programs. Hand calculations, however, are subject to error and hand plotting to bias. And while the saving in real time may have been negative, the saving in boredom was highly positive.

Although the use of the programs will be described in the next section, a few features common to all of them are given here. All programs were written in the Full Fortran IV language, compiled in Fortran G, and run on an IBM 360/65 computer. A listing of three of the programs (EC1, EC2, and EC5) may be found in Appendix B. The other two programs used are not given, since they merely involve reading in data to be graphed by the plotter. The subroutines PCLA (replace one polynomial by another), PDER (derivative of a polynomial), POLRT (roots of a polynomial), and PVAL (value of a polynomial) are not listed, as they are part of the IBM Scientific Subroutine Package (17). GRAPH, LETTER, and ORIGIN are part of a resident plotting routine SIMPLOTTER (18), and OPLSPA (19) is a resident curve fitting subroutine which calculates

least squares polynomial coefficients by an orthogonal polynomial method.

Method of Analysis

A general description of the method used to analyze the data will be given in this section. Complications obtained with individual adsorbates and the method of handling them will be discussed in the next section.

The first computer program used, ECl, converts the pressure readings to interfacial tension and fits the resulting electrocapillary data with an analytical expression. The expression chosen as the best fit to the data in each case was the least squares polynomial of highest degree (less than or equal to degree ten) which had no point of inflection in the region of the data¹. A complete description of ECl may be found in the listing of the program itself in Appendix B. An example of part of the output from the program is given in Appendix C and Figures 2-5.

When all the electrocapillary curves for a particular adsorbate had been analyzed by ECl, the polynomials fit to each curve were input to the second program, EC2. This program was used to shift the reference point of the potential

¹A portion of the electrocapillary curve with positive curvature would imply a negative differential capacity in that region, a physically untenable result.

scale from the saturated calomel electrode potential to that of the electrocapillary maximum of the base electrolyte. In addition the family of electrocapillary curves for the given adsorbate was plotted and the dependence of surface pressure, π (calculated from the least squares polynomials), on potential and ln activity was established. A listing of EC2 may be found in Appendix B.

For each potential (usually 50 millivolt intervals were chosen) a plot was made by the third program, EC3, of the surface pressure vs. In activity points. These plots were found to be superimposable (within experimental error) by shifting the entire graph horizontally along the ln a axis. One of the π -ln a curves, usually for a potential near the electrocapillary maximum, was chosen as a reference and the magnitude of the shift required for superposition, LNAINC, was found by eye and recorded as a function of potential.

The data thus obtained were read into the fourth program, EC4, which plotted all of the shifted π -ln a points on a single composite curve. An internal smoothing routine in SIMPLOTTER was used to plot a smooth curve through these points on a separate graph.

An interesting application of the superimposability of the surface pressure curves is a new method for determining solubility. A solution of known concentration is prepared and an electrocapillary curve of the solution taken. For each potential a value of the surface pressure, π , is calculated, and the ln a corresponding to this π is read from the composite π -ln a curve. When the shift for the given potential, LNAINC, is added to this ln a, the actual ln a of the solution is recovered. The activities obtained are averaged over a number of potentials, and the solubility, c_o , can then be calculated, since both c and $a = c/c_o$ are known. This method was used to determine the solubility of cyclohexanone.

In order to obtain the surface excess, Γ , the derivative of the composite π -ln a curve must be obtained. This may be done by graphical differentiation or by fitting the curve with a theoretical expression and differentiating analytically. Since the second method is more aesthetically pleasing, the surface pressure curve was tested against several different equations. The best fit to the data, however, was provided indirectly by the Frumkin isotherm, for which an analytical relation between π and ln a is impossible to obtain. In order to use a Frumkin isotherm, therefore, it was necessary to differentiate graphically the composite π -ln a curve to obtain Γ .

The computer-smoothed curve output from EC4 was found to contain several irregularities in slope, and was therefore resmoothed with French curves. Tangents to this curve were constructed, and two points were read from opposite ends

of each tangent. These points, along with the coordinates of the point on the curve to which the tangent was drawn, were used as part of the input data for the last computer program, EC5.

EC5 was written as a three-part program. The first section reads in actual data points from the linear portion of the composite π -ln a curve, which are then used to calculate the maximum surface excess, Γ_m (the surface excess corresponding to monolayer coverage). Next the points obtained in the graphical differentiation are read and converted first to surface excess, Γ , and then to fractional surface coverage, e. The array of ln a vs. θ points thus obtained is then fit with a Frumkin equation. The last part of the program reads in an array of potential vs. LNAINC points and these, together with the parameters of the Frumkin equation, are used to calculate the free energies of adsorption, ΔG_0^2 and ΔG_1^0 , as functions of potential.

Accuracy of Electrocapillary Curves

As was discussed in the experimental section, good precision was not obtained in the electrocapillary curves for several compounds because of the presence of impurities and loss of solute by evaporation. While nothing can be done ex post facto to regain the precision lost due to impurities, a semi-empirical method was developed to correct the data for evaporation losses. If it is assumed that the concentration

decays exponentially with time, as would be true for diffusional flow of vapor away from the surface for a simplified but nonetheless reasonable model, then

$$a = a_0 e^{-\alpha t}$$
, (18)

where a_0 and a are the bulk activities of the adsorbate at time 0 and t respectively, and α is the rate constant for the diffusion. The rate of change of interfacial tension, γ ,

$$\frac{\partial \gamma}{\partial t} = \left(\frac{\partial \gamma}{\partial \ln \alpha}\right) \left(\frac{\partial \ln \alpha}{\partial t}\right)$$

= $\left(-\Gamma_{m} RT \theta\right) (-\alpha)$ (19)

 $= A_{\theta}$

where $A = \alpha \Gamma_m RT$.

The fractional surface coverages, θ , were estimated by plotting preliminary π -ln a curves, forming a preliminary composite curve, and graphically differentiating. The constant A was estimated by plotting separate electrocapillary curves for the 100 mV and 50 mV interval points, and finding the difference, $\Delta\gamma$, between these curves at some potential. The time difference between the points on each curve was either known or estimated. The correction was then calculated for each data point and the data were corrected before submitting it to the program EC1.

The corrections applied, while small (see Table 1, Appendix D), greatly improved the precision of the electrocapillary data for chloroform and cyclohexanol. They were not applied to 3-pentanol, as the scatter due to impurities was too large to enable the constant A to be determined.

Another source of error was in the measurement of the height of the mercury column with the cathetometer. While the difference between individual readings was generally only a few hundredths of a millimeter, the heights of the mercury column measured on different days (even without expelling any mercury between measurements) sometimes differed by as much as a tenth of a millimeter, which would introduce an error of 0.05 dyne/cm in the interfacial tension. To minimize this error, a plot of mercury height vs. number of drops expelled from the capillary was made, and a straight line was drawn through the points. This straight line was then used to find both the mercury height at the start of <u>each</u> experiment, and the correction which was applied by EC1 to each data point for loss of mercury during the experiment.

Some error is undoubtedly introduced by attempting to fit the electrocapillary curve with a finite polynomial rather than an infinite series. An examination of the graphs produced by ECl, however, reveals that this error is within the scatter of the points in all cases. This means that the root mean square deviation of the data points from the polynomial fit to these points provides a good measure of the precision of the data. Table 1 lists the RMS deviation, along with other information on the precision of the

various electrocapillary curves.

The fit in some cases is so good that the capacity curves produced by double differentiation of the electrocapillary curve reproduce not only the shape of the capacity curves obtained by direct measurement, but also are close to being numerically correct. Figure 5 compares the capacity curve for pure 0.1 N $HClO_4$ obtained from electrocapillary measurements with that obtained directly, and the fit is seen to be remarkably good except near the ends of the curve, where the electrocapillary data are not sufficient to permit an accurate determination of the curvature.

Accuracy of Results

While the errors in the taking and fitting of the original data are naturally propagated to the final results, there are other errors which arise in the course of analyzing the data due to the imperfect methods used.

In the process of superimposing the π -ln a curves, which was done by eye, it was assumed that surface pressures near the electrocapillary maximum potential were the most accurate,¹ and the curves were shifted to superimpose in this region. It is believed that this assumption is justified by the

¹Any error caused by a mistake in the radius of the capillary would be smallest near the electrocapillary maximum potential of the base electrolyte since the calibration point was the electrocapillary maximum.

larger scatter in the points of the composite curves in the low π region. Possibly the curves could have been superimposed with less scatter in all regions had this assumption not been made, but no unbiased way was found to do this. At high positive or negative potentials the surface pressures were too low to obtain an accurate measure of the shift required for superposition. This was made difficult both because of the increased scatter in the low π region and the low slope of the curve.

Before drawing a smooth curve for the composite π -ln a data certain points were deleted. Points at high positive or negative potentials were omitted for 3-pentanol and cyclo-hexanol, as explained above. While only the 100 mV interval points are shown in Figures 10 and 12 for clarity, the 50 mV interval points were included when drawing the curve. For chloroform and cyclohexanone, larger regions were omitted due to the bad scatter of the points caused by impurities. In the case of chloroform the impurity was adsorbed mainly on the positive side of the electrocapillary maximum, while for cyclohexanone it was adsorbed on the negative side.

Possibly the largest sources of error in the analysis of the data were the inaccuracies inherent in drawing a smooth curve through the π -ln a points and in drawing tangents to this curve. Some of the bias in drawing the curve was eliminated by using the computer smoothing routine, but the graphical differentiation still caused considerable scatter

in the surface excesses obtained (see Figures 14-17). Although this scatter is large, the Frumkin isotherm which was fit to the data, when used to calculate theoretical π -ln a points, fit the original π -ln a points extremely well (see Figures 10-13).

Special problems arose in the analysis of the chloroform data due to its high volatility and low surface activity. When the π -ln a points were originally plotted it was discovered that they were all superimposable except the points for the saturated solution, which were superimposable on a different curve, parallel to the first but at higher surface pressure. Evidently considerable chloroform in the unsaturated solutions had evaporated during the process of preparing and mixing them, while any chloroform evaporating from the saturated solution during this process was replaced from the chloroform phase. Since the solutions had been prepared the day before the electrocapillary data were taken, and had been stirred overnight, considerable evaporation could have occurred around the stopper of the flask during In fact it was later found that if a flask this time. containing a saturated solution with a small lens of chloroform on the bottom was left standing for a few days, the lens would disappear.

- Since the π -ln a points for the lower concentrations were superimposable it was assumed, as for the previous evaporation correction, that the concentration decayed

exponentially with time. Since the time of evaporation was approximately the same for each solution, the π -ln a points were shifted by the same amount to a lower ln a. The composite curve thus obtained, while not as accurate due to the approximate method of correction, has a scatter comparable to that found for the other adsorbates studied.

Due to the low surface activity of chloroform, monolayer coverage was not approached even with a saturated solution. A special technique was therefore used to approximate the maximum surface excess. It was assumed that the data could be fit by a Frumkin isotherm, for which a plot of ln a vs. θ is symmetric on inversion through the point ($\theta = \frac{1}{2}$, ln a = ln $a_{\frac{1}{2}}$). A plot of the surface excess, Γ , vs. ln a was made, and the point of symmetry was determined by eye. Twice the value of Γ at this point was taken as the maximum surface excess.

Résults

Electrocapillary curves for the adsorbates studied are given in Figures 6-9. 3-pentanol, cyclohexanol, and cyclohexanone can be seen to shift the potential of the electrocapillary maximum to the right, indicating a preferential adsorption on a negatively charged surface. Chloroform, within experimental error, does not shift the potential of the electrocapillary maximum at all.
Coefficients of the polynomials fit to each electrocapillary curve were listed as part of the output data of program EC2. These are given in Appendix C, along with the coefficients of the polynomials after transformation to the new potential scale (volts vs. electrocapillary maximum). A table of interfacial tensions calculated from these polynomials is also given for each adsorbate.

The composite π -ln a points and the curve calculated from the Frumkin equation can be seen in Figures 10-13.

The output of program EC5 for each adsorbate (see Appendix C) lists the Frumkin parameters obtained, and a table of interfacial variables experimentally determined and those calculated from the Frumkin equation.¹

Rather than draw individual adsorption isotherms for each potential, it was found that if the dimensionless variables θ , fractional surface coverage, and a/a_1 , reduced activity², were used, a single isotherm was sufficient to describe the data at all potentials (see Figure 18). In fact, superimposability of the surface pressure plots is a sufficient condition for the existence of a single dimensionless isotherm. Superimposability implies that

¹The calculated values of π are not necessarily close to the experimental values, since they correspond to different activities.

 $^{^{2}}a_{\underline{1}}$ is the activity of the adsorbate in the bulk solution at one-half the maximum coverage.

$$\tilde{\pi} = f[\ln a + g(V)]$$
(20)

and that the fractional surface coverage is a function of π alone, independent of V, i.e. $\theta = h(\pi)$. Thus

$$\ln a = f^{-1}(\pi) - g(V)$$

= $f^{-1}[h^{-1}(\theta)] - g(V),$ (21)

or a is the product of two functions, one dependent on θ alone, the other on V alone, and hence $a/a_{\frac{1}{2}}$ will be independent of V.

This can be readily seen in the special case of the Frumkin isotherm, if Equation 7 is written in the form

$$\frac{\theta}{1-\theta} = B_0' \left(\frac{a}{a_{\frac{1}{2}}}\right) e^{2\alpha\theta} .$$
 (22)

 $a_{\underline{1}}$ is the only parameter which depends on the potential.

The standard free energies of adsorption ΔF_0^0 and ΔF_1^0 are plotted as a function of potential in Figures 21 and 22. These were calculated using Equations 16 and 15, where the B₀ for each potential was found from the relation

$$\ln B_{0} = \ln B_{0}' - \ln a_{\frac{1}{2}}$$

$$= \ln B_{0}' - \ln a_{\frac{1}{2}}' - \text{LNAINC}$$
(23)

where $\ln a_{\frac{1}{2}}$ is $\ln a_{\frac{1}{2}}$ for the reference potential of the composite surface pressure curve.

INTERPRETATION OF RESULTS

The fact that the π -ln a curves for the adsorbates studied can be superimposed means that the interactions between molecules of the adsorbate (as measured by the constant α of the Frumkin equation) are independent of potential. Only adsorbate-metal interactions (as measured by B₀ or the standard free energies of adsorption) are potential dependent. This is physically reasonable, as changing the electrical state of the interface would not be expected to have an appreciable effect on intermolecular forces. Parsons has observed superimposability¹ for a number of other compounds: thiourea (20, 21), sodium benzene m-disulfonate (22), n-butanol (23), and acetanilide (24).

The only compound known to this author for which the π -ln a curves are not superimposable² is phenol (16, 25). It is now believed (26) that there is an interaction between the electrode and the π -electrons of the benzene ring which causes the molecule to lie parallel to the surface when the mercury is positively charged. When the mercury is

¹Although Parsons has chosen the charge, rather than the potential as his electrical variable, he has shown (23) that within experimental error superimposability of the π -ln a curves is also possible if the potential is chosen.

²This does not mean to imply that other such compounds have not been observed, only that few authors have attempted superimposability.

negatively charged, the molecules undergo a gradual reorientation to a position perpendicular to the surface. This reorientation alters the molecular area at full coverage (and hence Γ_m), as well as the intermolecular forces. Although a Frumkin isotherm could be fit to the data for such a compound, the three parameters B_0 , α , and Γ_m would all vary with potential, and consequently would not be as easily interpretable.

It appears that unless some phenomenon such as reorientation occurs to change the intermolecular forces, these interactions should be independent of potential. Compounds for which molecular interactions are independent of the electrical state of the interface will henceforth be termed I-compounds, for brevity.

Previous work in this laboratory (14,16,25,27) has been analyzed by means of a generalized Frumkin isotherm

$$\frac{\theta}{1-\theta} = B_0' a e^{2\alpha\theta} e^{-(S\Psi/RT)}, \qquad (24)$$

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where S is the molar area of the adsorbate at full coverage,

$$\Psi = \int_{O}^{V} (\frac{\partial Q}{\partial \theta})_{V} dV ,$$

and the other parameters are as previously defined. Comparison of Equations 22 and 24 shows that

$$\Psi = \frac{RT}{S} \ln a_{\frac{1}{2}} .$$
(25)

For I-compounds, Φ has been shown to be a function of V alone (independent of Γ), and hence the surface charge density, Q, varies linearly with Γ (at fixed V), as was shown in Reference 25. Thus a linear variation of charge density with coverage appears to be justified for I-compounds. This is the basic assumption initially propounded by Frumkin (13), and used in this laboratory to obtain adsorption information from double layer capacitance measurements.

A comparison of the standard free energies of adsorption, $_{\Delta}G_{0}^{0}$ and $_{\Delta}G_{1}^{0}$, obtained for the various adsorbates studied should give an indication of the types of forces responsible for the adsorption. A model based on van der Waals forces which appears to represent the data fairly well has been published by Steele and Halsey (28). It is derived on the assumption of hard-sphere monolayer adsorption and applied to the adsorption of rare gas atoms on a solid surface. The formula which they obtain for the energy of interaction of an atom with the surface, ε^* , is

$$\epsilon^* = \frac{N_0 m c^2 \pi}{D^3} \left[\frac{\alpha_1 \alpha_2}{\frac{\alpha_1}{\chi_1} + \frac{\alpha_2}{\chi_2}} \right] , \qquad (26)$$

where N_0 is the number of adsorbent particles per cubic centimeter, m is the mass of the electron, c is the velocity of light, D is the distance of closest approach of adsorbate and adsorbent molecules, and α and χ are the polarizabilities and diamagnetic susceptibilities, respectively, of the

adsorbate and adsorbent molecules.

In applying this formulation to the mercury-solution interface we now have an adsorbent, Hg, and two adsorbates, water, w, and an organic substance, i. Thus

$$\epsilon_{\rm w} = \frac{N_{\rm o} {\rm mc}^2 \pi}{D_{\rm w}^3} \left[\frac{\alpha_{\rm Hg} \alpha_{\rm w}}{\alpha_{\rm Hg}} + \frac{\alpha_{\rm w}}{x_{\rm w}} \right]$$
(27)

and

$$\epsilon_{i} = \frac{N_{o}mc^{2}\pi}{D_{i}^{3}} \left[\frac{\alpha_{Hg}\alpha_{i}}{\alpha_{Hg}} + \frac{\alpha_{i}}{\chi_{i}}\right]$$
(28)

Now the change in interaction energy when one mole of organic solute replaces an equal area of water molecules is given by

$$\Delta E_{i} = -N \epsilon_{i} + N \epsilon_{w} \left(\frac{\overline{v}^{2/3}}{\overline{v}^{2/3}} \right) , \qquad (29)$$

where N is Avogadro's number, and \bar{V}_i and \bar{V}_w are the molar volumes of the organic substance and of water, respectively. It is assumed that since the model applies to hard-sphere adsorption, the ratio of the areas covered by the molecules is the same as the ratio of their molar volumes to the twothirds power.

Substituting Equations 27 and 28, dividing by $\bar{v}_1^{2/3}$, and assuming that the entropy term is negligible gives

$$-\frac{\Delta G_{1}}{\bar{v}_{1}^{2/3}} = \frac{k \alpha_{Hg}}{L_{1}} \left[\frac{\alpha_{1}}{\bar{v}_{1}^{2/3}} - \left(\frac{L_{1}}{L_{w}} \right) \frac{\alpha_{w}}{\bar{v}_{w}^{2/3}} \right], \qquad (30)$$

where $k = NN_0 mc^2 \pi$, $L_1 = D_1^3 \left(\frac{\alpha_{Hg}}{\chi_{Hg}} + \frac{\alpha_1}{\chi_1}\right)$, and $L_w = D_w^3 \left(\frac{\alpha_{Hg}}{\chi_{Hg}} + \frac{\alpha_w}{\chi_w}\right)$. The solutes investigated in this study were all organic molecules and all were found to adsorb with orientation parallel to the surface. In this circumstance their structures were such that D_1 should be nearly the same for all solutes. For these same solutes the ratio $\frac{\alpha}{\chi}$ varied from -33 x 10^6 to -44 x 10^6 c.g.s. units, and the ratio for mercury was about -30 x 10^6 c.g.s. units. Hence L_1 should be constant for these solutes within a range $\pm 10\%$. If L_1 is considered constant a plot of $-\frac{\Delta G_1}{\bar{\chi}^2/3}$ vs. $\frac{\alpha_1}{\bar{\chi}^2/3}$ should yield a straight line.

Such plots are given in Figures 21 and 22 for ΔG_0^0 and ΔG_1^0 at the potential of the electrocapillary maximum for the inert electrolyte. Points obtained for the four adsorbates studied are given, as well as points obtained for other adsorbates by previous workers in this laboratory through measurement of differential capacitance (14). The point for phenol on both graphs is clearly not on the line, which is to be expected since it was obtained by a method which assumed that it was an I-compound and it is not. While the model used is of course not strictly applicable to the mercury-solution system, the linearity of the plots suggests that van der Waals forces are of prime importance in adsorption at the mercury-solution interface.

The surface area occupied by a molecule of the adsorbate at full monolayer coverage may be obtained by taking the reciprocal of $\Gamma_{\rm m}$. Experimental surface areas are compared with those derived from molecular models in Table 2. Godfrey space-filling molecular models were arranged on a flat surface and photographed from directly above. Areas were then calculated assuming that the molecules were allowed to rotate about their geometric centers, and that they were arranged in a hexagonal array covering the surface.

Experimental surface areas can be seen in all cases to be somewhat larger than those obtained from the models, which is to be expected since the molecules are probably not localized in a regular array on the surface even at full coverage. The experimental areas of the larger molecules indicate that they are arranged parallel to the surface, rather than perpendicular. The hydroxyl group of cyclohexanol is most likely oriented in an equatorial position with respect to the ring. An anomaly in the case of cyclohexanone has yet to be explained.

Of the two main techniques used to obtain information on adsorption at the mercury-solution interface-interfacial tension and differential capacitance measurements-there has been considerable controversy in the literature (29-31) as to which is the more accurate. Most authors have compared the two methods by looking at the interfacial tension obtained directly from electrocapillary curves, γ_m , and that obtained indirectly by double integration of capacity curves, γ_c . Deviations between γ_m and γ_c are generally on the order of 0.5 dynes/cm, which is about the same as the experimental error of the measurements. Considering the greatly improved precision now obtainable in the measurement of γ_m , direct measurement would seem to be the preferable technique.

The use of a model based on the linear variation of Qwith Γ at constant V (14, 16, 25, 27) to infer adsorption from differential capacitance measurements has been justified for I-compounds. If capacitance data is used this technique would seem to be preferable to that of doubly integrating the capacitance data, since it would presumably involve less multiplication of errors.

SUMMARY

The adsorption of chloroform, 3-pentanol, cyclohexanol, and cyclohexanone at the mercury-0.1N perchloric acid solution interface has been studied. Interfacial tension measurements were made with a capillary electrometer of greatly improved precision.

In the analysis of the electrocapillary data_obtained for each adsorbate it was discovered that the surface pressure - ln activity curves for different potentials could be superimposed by a translation along the ln a axis. Implications of this superimposability are (1) that the interactions between molecules of the adsorbate are independent of the electrical state of the interface and (2) that the surface charge density varies linearly with surface excess (at fixed potential).

The Frumkin isotherm was used to fit the data for each adsorbate, and two standard free energies of adsorption were calculated from its parameters, one referring to standard states based on infinite dilution both in solution and on the surface and the other referring to standard states based on pure adsorbate both in solution and on the surface. A correlation between these standard free energies of adsorption and polarizabilities of the molecules was established, indicating that van der Waals forces are primarily responsible for the adsorbate-adsorbent

interactions.

Molecular areas determined experimentally were found to compare favorably with those obtained from molecular models.

The high precision of the interfacial tension measurements obtained would seem to favor direct measurement, rather than inference from capacitance measurements, as the more accurate method of obtaining adsorption parameters.

SUGGESTED MODIFICATIONS AND EXTENSIONS

Several experimental modifications should be made to increase both the accuracy and precision of the data. In order to study compounds of high volatility, an apparatus should be constructed to prepare the solutions from the saturated solution directly in the cell, to avoid loss of solute by evaporation during the mixing and transferring of the solution. Kaganovich, Gerovich, and Gusakova (32) have recently designed and used such an apparatus to find the electrocapillary curves of several volatile adsorbates.

Since even minute amounts of a surface active impurity can affect the accuracy of the electrocapillary data, the impurities remaining after distillation should be removed by a gas chromatographic separation.

It would be instructive to retake a family of electrocapillary curves for one of the adsorbates already studied and note any difference in the results obtained after these two modifications. If these modifications cause a significant improvement in the accuracy of the data, a critical comparison should be made between analyses of the data using potential and using charge as the electrical variable. It is possible that improved precision could enable a decision to be made in this continuing controversy (10, 23, 24, 33-37).

With data of improved accuracy it would be interesting

to see if fitting the electrocapillary curves in sections, rather than as a whole, would cause a better correspondence between capacitance curves obtained directly and those obtained by double differentiation of electrocapillary curves. A computer program to fit the electrocapillary curve in sections has been recently written by Mohilner (38).

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BIBLIOGRAPHY

1.	G. Lippmann, Ann. chim. phys., (5) <u>5</u> , 494 (1875).
2.	G. Gouy, Ann. chim. phys., (7) <u>29</u> , 145 (1903).
3.	G. Gouy, Ann. chim. phys., (8) <u>8</u> , 291 (1906).
4.	G. Gouy, Ann. chim. phys. (8) <u>9</u> , 75 (1906).
5.	G. Gouy, J. phys. radium, (4) <u>9</u> , 457 (1910).
6.	G. Gouy, Compt. rend., <u>149</u> , 654 (1910).
7.	D. C. Grahame, Chem. Rev., <u>41</u> , 441 (1947).
8.	R. Parsons, Advances in Electrochem. and Electrochem. Eng., $\underline{1}$, 1 (1961).
9.	B. B. Damaskin, Russian Chemical Reviews (Uspekhi Khimii), <u>30</u> , 78 (1961).
10.	B. B. Damaskin, Russian Chemical Reviews (Uspekhi Khimii), <u>34</u> , 752 (1965).
11.	M.A.V. Devanathan and B.V.K.S.R.A. Tilak, Chem. Rev., <u>65</u> , 635 (1965).
12.	P. Delahay, Double layer and electrode kinetics, New York, N.Y., Interscience Publishers (1965).
13.	A. N. Frumkin, Z. Physik, <u>35</u> , 792 (1926).
14.	R. S. Hansen, R. E. Minturn and D. A. Hickson, J. Phys. Chem., <u>61</u> , 953 (1957).
15.	C. A. Smolders and E. M. Duyvis, Rec. Trav. Chim., <u>80</u> , 635 (1961).
16 <i>.</i>	D. J. Kelsh, The deformation of the electrocapillary curve due to adsorption of organic molecules, Unpublished Ph.D. thesis, Ames, Iowa, Library, Iowa State University of Science and Technology (1962).
17.	IBM, System/360 Scientific Subroutine Package [360A-CM- 03X], Programmer's Manual H20-0205-0 (1966).

- D. G. Scranton, SIMPLOTTER, Computer Utilization Bulletin No. 23, Ames, Iowa, Library, Ames Laboratory, U.S.A.E.C. (ca. 1966).
- 19. J. E. Delany, Subroutine OPLSPA, Unpublished paper, Mimeographed, Ames, Iowa, Library, Ames Laboratory, U.S.A.E.C., Distribution No. 360400266110003 (1966).
- 20. R. Parsons, Proc. Roy. Soc. (London), <u>A261</u>, 79 (1961).
- 21. E. Dutkiewicz and R. Parsons, J. Electroanal. Chem., <u>11</u>, 196 (1966).
- 22. J. M. Parry and R. Parsons, Trans. Faraday Soc., <u>59</u>, 241 (1963).
- 23. R. Parsons, J. Electroanal. Chem. <u>8</u>, 93 (1964).
- 24. R. Parsons and F. G. R. Zobel, Trans. Faraday Soc., <u>62</u>, 3511 (1966).
- 25. R. S. Hansen, D. J. Kelsh and D. H. Grantham, J. Phys. Chem., <u>67</u>, 2316 (1963).
- 26. B. B. Damaskin, V. M. Gerovich, I. P. Gladkikh and R. I. Kaganovich, Russian J. Phys. Chem. (Zh. Fiz. Khim.), <u>38</u>, 1351 (1964).
- 27. R. S. Hansen, R. E. Minturn, D. A. Hickson, J. Phys. Chem., <u>60</u>, 1185 (1956).
- 28. W. A. Steele and G. D. Halsey, Jr., J. Chem. Phys., <u>22</u>, 979 (1954).
- 29. J. O'M. Bockris, K. Muller, H. Wroblowa and Z. Kovac, J. Electroanal. Chem., <u>10</u>, 416 (1965).
- 30. R. Payne, J. Electroanal. Chem., <u>15</u>, 95 (1967).
- 31. J. O'M. Bockris, K. Muller, H. Wroblowa and Z. Kovac, J. Electroanal. Chem., <u>15</u>, 101 (1967).
- 32. R. I. Kaganovich, V. M. Gerovich and O. Yu. Gusakova, Soviet Electrochem. (Electrokhimiya), <u>3</u>, 836 (1967).
- 33. R. Parsons, Trans. Faraday Soc., <u>51</u>, 1518 (1955).
- 34. J. O'M. Bockris, M. A. V. Devanathan, K. Muller, Proc. Roy. Soc. (London), <u>A274</u>, 55 (1963).

- 35. R. Parsons, J. Electroanal. Chem., 7, 136 (1964).
- 36. B. B. Damaskin, J. Electroanal. Chem., 7, 155 (1964).
- 37. A. N. Frumkin, B. B. Damaskin and A. Survila, J. Electroanal. Chem., <u>16</u>, 493 (1968).
- 38. D. M. Mohilner and P. R. Mohilner, J. Electrochem. Soc., <u>115</u>, 261 (1968).

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Special thanks must also go to Gordon Potter, who designed most of the experimental apparatus used.

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APPENDIX A

Figures Cited in Text

The numerical data corresponding to the graphs of Figures 2 - 18 may be found in Appendix C.

Figure 1 Diagram of apparatus

- Figures 2-5 Example of output from computer program EC1
- Figures 6-9 Electrocapillary curves
- Figures 10-13 Composite π -ln a curves
- Figures 14-17 ln a vs. θ curves
- Figure 18 Adsorption isotherms
- Figures 19-20 Free energy vs. potential curves
- Figures 21-22 Correlation of free energy with polarizability

Figure 1. Diagram of apparatus. Four mercury cells are used to supply a potential to the potentiometer, which applies a known potential between the mercury in the capillary and the saturated calomel electrode used as a reference. Pressure is applied to the gas above the mercury by a set of screw-driven glass syringes, and is measured with the fused quartz precision pressure gauge. The capillary is viewed through a binocular microscope (not shown) set in front of the cell.

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Figure 2. Example of an electrocapillary curve output from computer program EC1. The solution used was $0.100 \text{ N} \text{ HC10}_4$ with no organic adsorbate present. Points shown are experimental data. The curve is the least squares polynomial fit to the data.

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Figure 3. The region of the electrocapillary curve of Figure 2 near the electrocapillary maximum, shown on an expanded scale.

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Figure 4. Surface charge per unit area on the mercury side of the double layer. The curve is calculated from the least squares polynomial fit to the electrocapillary data of Figure 2.



Figure 5. Differential capacitance per unit area of the double layer. Points shown are direct experimental data. The curve is calculated from the least squares polynomial fit to the electrocapillary data of Figure 2.

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Figure 6. Electrocapillary curves for 3-pentanol in 0.100N HClO₄. Concentrations of 3-pentanol are (A) zero; (B) 0.0131M; (C) 0.0263M; (D) 0.0525M; (E) 0.133M; (F) 0.263M; (G) 0.588M.



Figure 7. Electrocapillary curves for chloroform in 0.100N HClO₄. Concentrations of chloroform are, from the top curve down, zero; 0.0126M; 0.0178M; 0.0251M; 0.0316M; 0.0377M; 0.0455M; 0.0460M; and 0.0494M.



Figure 8. Electrocapillary curves for cyclohexanol in 0.100N HClO₄. Activities of cyclohexanol are (A) zero; (B) 0.025; (C) 0.050; (D) 0.100; (E) 0.225; (F) 0.450; (G) 0.900.



Figure 9. Electrocapillary curves for cyclohexanone in 0.100N HClO₄. Activities of cyclohexanone are (A) zero; (B) 0.025; (C) 0.050; (D) 0.100; (E) 0.238; (F) 0.475; (G) 0.950. Data for curves B and D were obtainable only for the regions shown. Data for curve C are unreliable to the left of the electrocapillary maximum.

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Figure 10. Composite π -ln a curve for 3-pentanol. Points are experimental data; the line is calculated from the Frumkin equation fit to the data. In the legend above, the first number is the potential, V, in volts vs. the electrocapillary maximum potential for 0.100N HClO₄. The number in parenthesis is the amount by which the ln a axis has been shifted with respect to the curve for -0.033 volts.

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Figure 11. Composite π -ln a curve for chloroform. Legend as in Figure 10, except that the reference was the curve for 0 volts.

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Figure 12. Composite π -ln a curve for cyclohexanol. Legend as in Figure 11.

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Figure 13. Composite π -ln a curve for cyclohexanone. Legend as in Figure 10, except that the potential, V, is in volts vs. S.C.E. and the reference was the curve for -0.7 volts.

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Figure 14. In a vs. θ curve for 3-pentanol. θ is the fractional surface coverage, Γ/Γ_m . Points shown were obtained by graphical differentiation of the composite π -ln a curve. The line is calculated from the Frumkin equation fit to the points.



Figure 15. In a vs. θ curve for chloroform.

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Figure 16. In a vs. θ curve for cyclohexanol.



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Figure 17. In a vs. θ curve for cyclohexanone.



Figure 18. Dimensionless adsorption isotherms. $a_{\frac{1}{2}}$ is the activity of the absorbate at which $\theta = \frac{1}{2}$. Adsorbates shown are (A) chloroform, (B) cyclohexanol, (C) 3-pentanol, and (D) cyclohexanone.



Figure 19. Standard free energy of adsorption referred to infinite dilution based standard states both in solution and on the surface. Adsorbates shown are (A) cyclohexanone, (B) cyclohexanol, (C) 3-pentanol, and (D) chloroform.

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Figure 20. Standard free energy of adsorption referred to pure solute based standard states both in solution and on the surface. Adsorbates shown are (A) cyclohexanone, (B) cyclohexanol, (C) 3-pentanol, and (D) chloroform.







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Figure 22. Correlation of ΔG_1^O with polarizability, α . Points are numbered as in Figure 21.



APPENDIX B

Computer Program Listings

- EC1 Program for initial analysis of electrocapillary data. Page 94
- EC2 Second program for analysis of electrocapillary data. Page 107
- EC5 Program for fitting Frumkin equation to electrocapillary data from a composite π -ln a curve Page 112

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PROGRAM FOR INITIAL ANALYSIS OF ELECTROCAPILLARY DATA С С С USE OF PROGRAM С RAW ELECTROCAPILLARY DATA FCR THE PROGRAM MAY BE OF C THREE TYPES. AS INCICATED BY THE PARAMETER IDATA. С GAS PRESSURE MEASURED WITH MANCMETER ICATA = 1С = 2 GAS PRESSURE MEASURED WITH BOURDON С TUBE PRESSURE GAUGE C DATA ALREADY CONVERTED TO DYNES/CM = 3 C C C THE PROGRAM MAY BE USED TO CALCULATE THE RADIUS OF THE CAPILLARY IF DATA ARE TAKEN FOR A SOLUTION OF KNOWN ELECTRICCAPILLARY MAXIMUM, OR IT MAY BE USED С TO CALCULATE THE INTERFACIAL TENSION AT EACH DATA С POINT IF THE RADIUS IS ALREADY KNOWN. С DATA ARE NCT FOR CALIBRATION: RADIUS ICALIB = 0С = RADIUS OF CAPILLARY IN CM. C ICALIB = 1DATA ARE FCR CALIBRATION CF С CAPILLARY; RADIUS = E.C.MAX. OF C SCLUTION (CYNES/CM). С С METHOD THE PROGRAM FIRST FINDS THE PRESSURE ON THE С С INTERFACE FOR EACH CATA POINT (IF IDATA = 1 OR 2). С AND THEN CONVERTS THIS TO INTERFACIAL TENSION (IF С IN EITHER CASE, WHETHER THE FINAL ICALIB = 0)С RESULTS ARE PRESSURE OR INTERFACIAL TENSION, THE С ARRAY IS LAVELLED Y, AND THE DATA (VOLTS, Y) ARE С THEN FIT WITH A LEAST SQUARES POLYNOMIAL (FOR A С DEFINITION OF "BEST FIT", SEE SUBROUTINE FITECC). С WEIGHTING FACTORS ARE ASSIGNED TO EACH DATA PCINT BY FITTING THE CIFFERENCES BETWEEN EXPERIMENTAL С С AND CALCULATED Y'S WITH A NORMAL ERROR CURVE, AND С THE DATA ARE FIT AGAIN USING THESE WEIGHTS. A PLOT С OF THE CALCULATED ELECTROCAPILLARY CURVE WITH С SUPERIMPOSED EXPERIMENTAL PCINTS IS MADE, AS WELL С AS A PLOT OF THE REGION NEAR THE E.C.MAX. IF THE CATA WERE NOT USED FCR A CALIBRATION, THE CHARGE С DENSITY, Q, AND THE DIFFERENTIAL CAPACITANCE OF THE С С DOUBLE LAYER, C, ARE CALCULATED FROM THE POLYNOMIAL С FIT AND PLOTTED, AND THE COEFFICIENTS OF THE С POLYNOMIAL ARE PUNCHED ON DATA CARDS FOR USE IN THE С IF THE DATA WERE USED FOR A NEXT PROGRAM. CALIBRATICN, THE RADIUS OF THE CAPILLARY IS FOUND. С С С DESCRIPTION OF CATA CARDS С ALL CATA MUST BE IN CGS UNITS, UNLESS OTHERWISE С NOTED. С INITIAL CARDS (CNLY ONE SET, AT BEGINNING OF RUN): С CARD 1 (3F10.0): GRAV - ACCELERATION OF GRAVITY, С DHG - DENSITY CF MERCURY, DH20 - DENSITY OF

WATE R.
CARD 2 (2F15.0): BOURC(1) AND BOURD(2) - COEFS.
(IN ASCENDING POWER OF DOD) OF THE LINEAR
APPROX. TO THE BOURDON TUBE CONSTANT, IN INCHES
OF HG PER DEGREE OF DEFLECTION.
CARD 3 (3F1C.C): CMICR - CALIBRATION CONSTANT OF
THE MICROSCOPE RETICLE USED TO POSITION THE HG
SURFACE IN THE CAPILLARY, IN CM/DIVISION, DIV ~
UISTANLE UP HE SUKFALE FRUM BUTTUM LF CADILLADY IN DIVISIONS ON MICDOSCODE DETICLE
DADIUS - EVPLAINED ABOVE
CADIOS - EXPERINED ACOVES
CARD 5 (315): IDATA. ICALTB. MSTART - LOWEST
DEGREE POLYNOMIAL TO BE FIT TO DATA.
CARES FOR EACH DATA SET:
CARDS 6 E 7 (20A4/20A4): TITLE
CARD 8 (15A4): ORG, ELECTR, DATE - TITLES FOR
GRAPHS (MUST BE 20 CHARACTERS EACH, STARTING IN
COLUMNS 1, 21, AND 41).
CARD 9 (4F10.0): (OMIT IF IDATA = 3) TOPHG,
WATER, BCTCAP - CATHETOMETER READINGS OF THE
TOP OF THE HG COLUMN BEFORE CATA WAS TAKEN, THE
LEVEL OF THE SOLUTION IN THE CELL, AND THE
BOTTOM OF THE CAPILLARY, CORR - DECREASE IN HG
HEIGHT PER CROP OF HG EXPELLED.
CARUS 10 10 (N-2) (4F10.0): DATA FUR EACH PUINT
OF THE ELECTRUCAPILLART GURVE (MUST DE IN URDER FROM SMALLEST TO LARCEST ROTENTIAL NEED NOT
PROMISMALLEST TO LANGEST PUTENTIAL NEED NOT
TE INATA = 1 * VOLTS - ADDITENTIAL.
MANTOP - READING OF TOP MANOMETER COLUMN.
MANBOT - READING OF BOTTOM MANOMETER COLUMN.
CROPS - NC. CF DROPS OF HG EXPELLED SO FAR.
IF IDATA = 2: VOLTS, DOD - DEGREES OF
DEFLECTION ON BOURDON TUBE PRESSURE GAUGE,
DROP S .
IF IDATA = 3: VOLTS, Y - INTERFACIAL TENSION
CARD (N-1): BLANK CARD, TO INCICATE END OF ABOVE
ARRAY
CARC N (15): NDATA - NUMBER OF THE DATA SET
(LAST DATA SET MUST FAVE NDATA = 0)
CCMMCN NOTS, VOLTS(100), V(100), W(100), VCCE(11),
1 PYCOF(10), DDVCOF(9), PMC, WITCOT, TCCF(11),
2 MDEG. VEST(100), ERROR(100), CRG(5), ELECTR(5),
3 WTFACT(5) • DATE(5) • MSTART • Z
DIMENSION TDEG(10), DEG(5), TYLP(5), TYLG(5), TWTF1(5),
1 TWTF2(5), GL(5), SCALE(5), GLQ(5), YLQ(5),

```
GLC(5), YLC(5), BOURD(2), XL(5), TITLE(40),
     2
     3
                  DROPS(100), DOD(10C), YL(5), VEXP(100),
                  YEXP(100), YESTEX(100), QCOF(10), CCOF(9),
     4
     5
                  Q(100), C(100)
      INTEGER Z, $
            MANTOP(100), MANBOT(100)
      REAL
      EQUIVALENCE
                   (MANTOP, DOD, Q, VEXP), (MANBOT, C, YEXP),
                    (DROPS,W), (DYCOF,QCOF), (DDYCOF,CCOF)
     1
С
С
 1001 FORMAT (4F10.0)
 1002 FCRMAT (2F15.0)
 1003 FORMAT (2044/2044)
 1004 FORMAT (315)
 2001 FORMAT (15A4)
 2CC2 FORMAT (1P4E15.7)
 3001 FORMAT ("1"///1X,20A4/2X,20A4)
3002 FORMAT (// INPUT PARAMETERS )
 3003 FORMAT (/4X, 'GRAV', 6X, 'DFG', 8X, 'DH20'/F10.2, F11.4, F11.5)
3004 FORMAT (/4X, BOURC(1), 8X, BOURC(2) / 2F16.6)
 3005 FORMAT (/4X, CMICR', 6X, DIV', 4X, RADILS'/F11.5, F7.1,
     1 1PE14.4
 3006 FORMAT (/4X, "XL "/4X, 5A4)
3007 FORMAT (/4X, "IDATA", 4X, "ICALIP", 4X, "MSTART"/I5, 19, 110)
3008 FORMAT (/4X, 'ORG', 20X, 'ELECTR', 17X, 'DATE'/4X, 5A4, 3X, 5A4,
     1 3X_{1}5A4
3 CO9 FORMAT (/// DATA PCINTS (GAS PRESSURE MEASURED WITH ",
     1 "MANOMETER)")
3010 FORMAT (/6X, 'TOPHG', 5X, 'WATER', 5X, 'BOTCAP', 7X, 'CCRR'/
     1 F12.3,2F10.3,F14.7)
3011 FORMAT (/6X, VOLTS', 4X, MANTOP', 4X, MANBCT', 4X, DROPS'/
     1 (F11_{\bullet}3, 2F10_{\bullet}3, F8_{\bullet}0))
3012 FORMAT (/// DATA POINTS (GAS PRESSURE MEASURED WITH ".
     1 "BOURCON GAUGE)")
3013 FORMAT (/6X, "VOLTS", 6X, "DOD", 6X, "DROPS"/(2F11.3, F8.0))
3014 FORMAT (///' DATA PCINTS (IN DYNES/CM)')
3015 FORMAT (/6x, 'VOLTS', 7x, 'Y'/(2F11.3))
3016 FORMAT ( 11 //// OUTPUT CATA / VOLTS = EMF IN 1,544/
     1 6X, Y = .5A4
3C17 FORMAT (*1*////* BEST FIT TO CATA FOR *,5A4,1X,5A4,1X,
     1 5A4/1X, 5A4
                  PCLYNCMIAL OF DEGREE ',12,' WAS BEST FIT.'/
3018 FORMAT (/*
     1 •
         RMS CEVIATION = +,F5.31
3019 FORMAT (/5x, VOLTS', 4x, 'Y(EXPTL)', 4X, 'Y(CALCD)', 5X,
     1 'ERROR'/(F10.3,F11.3,F12.3,F11.3))
3020 FORMAT (*1*)
3021 FORMAT (/5x, VCLTS, 4x, WEIGHT, 4x, Y(EXPTL), 4x,
     1 'Y(CALCD)',5X,'ERROR',7X,'Q',8X,'C'/(F10.3,F9.3,F12.3,
     2 F12.3,F11.3,F10.2,F9.2))
3C22 FORMAT (/* RADIUS OF CAFILLARY = *, 1PE12.6)
```

3023 FORMAT (/5x, " VOL TS ", 4X, " WEIGHT ", 4X, " Y (EXPTL) ", 4X, 1 'Y(CALCC)',5X, 'ERROR'/(F10.3,F5.3,F12.3,F12.3,F11.3)) 3024 FORMAT (COORDINATES OF ELECTRCCAPILLARY MAXIMUM ARE " 1 '(',F6.3,',',F7.3,')') 3025 FORMAT (NO MAXIMUM WAS FOUND IN REGION OF DATA,) С С PUT ALPHANUMERIC DATA INTO ARRAYS FOR GRAPH LABELS. С С DATA TDEG(3)/4H3RC /, TDEG(4)/4H4TH /, TDEG(5)/4H5TH /, Ζ TDEG(6)/4H6TF /,TDEG(7)/4H7TH /,TDEG(8)/4H8TH /, TDEG(9)/4H9TH /, TDEG(10)/4H10TH/, DEG(2)/4H DEG/, 1 2 CEG(3)/4H. PO/, DEG(4)/4HLYN0/, DEG(5)/4HMIAL/, 3 TYLP /20HPRESSURE (CM OF HG) /. 4 TYLG /20HGAMMA (DYNES/CM) 1, 5 TWTF1/20H NO WEIGHTS USEC 1. 6 TWTF2/20H WEIGHTS WERE USED 1. 7 GŁ /20HE.C. CURVE FOR /, 8 SCALE/20HREGION NEAR E.C.MAX./, GLQ /20HCHARGE ON FG Ģ 1, A YLO /20HQ (MICROCOUL/CM++2) /, B GL C /20HCAPACITANCE OF D.L. /. С. YLC /20HC (MICROFARAD/CN**2)/ С С WITH THE PROPER CONTROL CARDS, SETTING Z AND \$ = 13 C WILL CAUSE ALL WRITE STATEMENTS WITH A Z OR \$ TO BE С OUTPUT ON THE PRINTER, AND WILL CAUSE ALL PROGRAM С INTERRUPT STATEMENTS NOT TO BE OUTPUT. SETTING Z = 3 С WILL CAUSE ALL WRITE STATEMENTS WITH A Z NOT TO BE С OUTPUT (USE FOR FINAL WHITE PAPER JOBS). С 2 = 3**s** = 13 С С READ INITIAL DATA CARDS. С READ (1,1001) GRAV,DFG,DH20 READ (1,1002) BCURD(1), BOURD(2) READ (1,1CO1) CMICR, DIV, RADIUS READ (1,1003) XL READ (1,1004) IDATA, ICALIB, MSTART С С READ TITLE, SYSTEM, DATE & PRINT ALL INPUT DATA SO С FAR. С 1 READ (1,1003) TITLE, ORG, ELECTR, DATE WRITE (Z,3001) TITLE WRITE (Z,3002) WRITE (Z,3003) GRAV, DHG, CH20 WRITE (Z,3004) BOURD(1),BOURC(2)

```
С
С
С
С
С
```

```
TEST FOR TYPE OF DATA TO BE READ, READ POINTS,
         CALCULATE Y.
      GO TO (2.8.14), IDATA
         GAS PRESSURE WAS MEASURED WITH MANCHETER.
С
С
    2 WRITE (Z,3009)
      READ (1,1001) TCPHG, WATER, BOTCAP, CORR
      WRITE (Z,3010) TCPHG, WATER, BOTCAP, CORR
      DO 3 I=1,1CO
      READ (1,1001) VOLTS(I), MANTOP(I), MANBCT(I), DROPS(I)
      IF (VOLTS(I) + MANTOP(I) + MANBOT(I)) 3, 4, 3
    3 \text{ NPTS} = I
    4 WRITE (Z,3011) (VCLTS(I),MANTOP(I),MANBOT(I),DROPS(I),
     1 I=1, NPTS
      PRES = TOPHG - BOTCAP - DIV * CMICR - (WATER - BOTCAP -
     1 DIV + CMICR) + DH20 / DHG
      DO 5 I=1,NPTS
    5 Y(I) = PRES + MANTCP(I) - MANECT(I) - CORR * DROPS(I)
С
      IF (ICALIB) 6,6,18
    6 CCNST = CHG * GRAV * RADIUS / 2.0
      DO 7 I=1,NPTS
    7 Y(I) = CCNST + Y(I)
      GO TO 17
С
         GAS PRESSURE MEASURED WITH BOURDON GAUGE.
С
С
    8 WRITE (Z,3012)
      READ (1,1001) TCPHG, WATER, BUTCAP, CORR
      WRITE (Z,3010) TOPHG, WATER, BCTCAP, CORR
      DO 9 I=1,1CO
      READ (1, 1001) VOLTS(1), DOD(1), DROPS(1)
      IF (VCLTS(I) + DOD(I)) 9, IO, 9
    9 \text{ NPTS} = I
   10 WRITE (Z, 3013) (VGLTS(I), DOD(I), DROPS(I), I=1, NPTS)
      PRES = TOPHG - BOTCAP - DIV + CMICR - (WATER - BOTCAP -
     1 DIV * CMICR) * DH20 / DHG
      DO 11 I=1.NPTS
      BCUR = BOURD(1) + BOURD(2) + COD(1)
   11 Y(I) = PRES + 2.540005 * BOUR * COC(I) - COPR * CROPS(I)
С
      IF (ICALIB) 12,12,18
   12 CENST = DHG * GRAV * RADIUS / 2_{\bullet}0
```

WRITE (Z,3005) CMICR, DIV, RADIUS

WRITE (2,3007) IDATA, ICALIB, MSTART WRITE (2,3008) ORG, ELECTR, DATE

WRITE (2,3006) XL

```
DO 13 I=1, NPTS
    13 Y(I) = CONST * Y(I)
       GO TO 17
С
С
          DATA ALREADY IN DYNES/CM.
С
    14 WRITE (Z,3014)
       DO 15 I=1,100
       READ (1,1001) VOLTS(I), Y(I)
       IF (VOLTS(I) + Y(I)) 15,16,15
   15 \text{ NPTS} = I
   16 WRITE (Z,3015) (VOLTS(I),Y(I), I=1,NPTS)
С
С
          PUT TITLE FOR Y-AXIS INTO YL ARRAY.
С
   17 DO 171 I=1,5
  171 YL(I) = TYLG(I)
       GC TO 20
   18 DO 19 I=1,5
   19 YL(I) = TYLP(I)
С
Č
C
          PRINT TITLE FOR OUTPUT DATA, SET WEIGHTS = 1.0, PUT
          TITLE INTO WTFACT ARRAY.
С
   20 WRITE (Z, 3016) XL, YL
       DO 21 I=1,NPTS
   21 W(I) = 1.0
      DO 22 I=1,5
   22 \text{ WTFACT(I)} = \text{TWTF1(I)}
С
С
          FIT PCLYNOMIAL TO CATA (VOLTS, Y), PRINT RESULTS.
С
      CALL FITECC
      WRITE (Z,3017) ORG, ELECTR, DATE, WTFACT
      WRITE (Z,3018) MDEG, RMS
      IF (VMAX + YMAX) 40.41.40
   41 WRITE (Z, 3025)
      GO TC 42
   4C WRITE (Z, 3024) VMAX, YMAX
   42 WRITE (Z,3019) (VOLTS(I), Y(I), YEST(I), ERROR(I), I=1, NPTS)
      WRITE (Z,3020)
С
С
          CALCULATE WEIGHTS, PUT NEW TITLE INTO WTFACT ARRAY,
          FIT NEW POLYNOMIAL TO DATA, PRINT INITIAL RESULTS.
С
С
      DO 23 I=1, NPTS
   23 \text{ W}(I) = 0.3989423 * \text{EXP} \left( (\text{ERROF}(I)/\text{WTRMS}) * 2 / (-2.) \right)
      DO 24 I = 1.5
   24 \text{ wTFACT(I)} = TwTF2(I)
      CALL FITECC
```

```
99
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```
WRITE ($,3017) ORG, ELECTR, DATE, WTFACT
     WRITE ($,3018) MDEG, RMS
     IF (VMAX + YMAX) 43,44,43
   44 WRITE ($,3025)
     GO TC 45
   43 WRITE ($,3024) VMAX, YMAX
С
        GRAPH CALCULATED E.C. CURVE AND DATA POINTS.
С
С
   45 VSIZE = AINT ((VCLTS(NPTS) ~ VCLTS(1)) / 0.2 + 2.0001)
     VO = VSIZE - 2.0
     DEG(1) = TCEG(MDEC)
     CALL GRAPH (NPTS, VOLTS, YEST, 0, 2, VSIZE, 10., 0, 0, 0, 0, XL, YL,
    1 GL, ORG)
     CALL GRAPH (NPTS, VOLTS, Y, 1, 7, C, 0, 0, 0, C, 0, 0, 0, 0, 0)
     1 C)
     CALL LETTER (V0,9.05,0.1,DATE,0.,20,0,0,0,0,0,0,0,C,C,0,0)
     CALL LETTER (V0,8.80,0.1,DEG,C.,2C,0,0,0,0,0,0,0,0,0,0)
С
        GRAPH REGION NEAR E.C. MAXIMUM.
С
С
     IF (VMAX + YMAX) 25,30,25
   25 YEXPC = AINT (YMAX - 9_{\bullet}0)
     J = 0
     DO 26 I=1, NPTS
     IF (Y(I) - YEXPO) 26,27,27
   27 J = J + 1
     VEXP(J) = VOLTS(I)
     YEXP(J) = Y(I)
     YESTEX(J) = YEST(I)
   26 CONTINUE
     VEXPSZ = AINT ((VEXP(J) - VEXP(1)) / C_005 + 2.00C1)
     VEO = VEXPSZ - 2.0
     CALL GRAPH (J,VEXP,YESTEX,0,2,VEXPSZ,10,0,0,0,0,XL,YL,
    1 GL, CRG)
     CALL GRAPH (J, VEXP, YEXP, 1, 7, 0, C, C, 0, 0, 0, 0, 0, 0, 0)
     1 0)
     1 C)
     CALL LETTER (VE0,8.80,0.1,DEG,C.,2C,0,0,0,0,0,0,0,0,0,0,0)
     1 0)
С
   30 IF (ICALIB) 31,31,34
С
       FIND CHARGE AND CAPACITANCE.
С
С
   31 \text{ OCCF(MDEG)} = -0.1 + CYCOF(MOEG)
```

```
MDEG1 = MDEG - 1
      DC 32 J=1, MDEG1
      QCOF(J) = -0.1 * CYCCF(J)
   32 CCOF(J) = -0.1 * DDYCOF(J)
      DO 33 I=1, NPTS
     CALL PVAL (Q(I), VOLTS(I), QCOF, MDEG)
   33 CALL PVAL (C(I), VOLTS(I), CCOF, MDEG1)
C
С
        PRINT FINAL RESULTS, GRAPH Q AND C.
С
     WRITE ($,3021) (VCLTS(I),W(I),Y(I),YEST(I), ERROR(I),
     1 Q(I), C(I), I=1, NPTS)
     CALL GRAPH (NPTS, VOLTS, Q.0.2, VSIZE, 10.0, 0, 0, 0, XL, YLQ,
    1 GLQ, ORG)
     1 0)
     CALL GRAPH (NPTS, VOLTS, C,0,2,VSIZE, 10,0,0,0,0,XL,YLC,
    1 GLC, ORG)
     1 0)
С
С
        PUNCH DATA CARCS FOR NEXT PROGRAM.
С
     MDEG1 = MDEG + 1
     WRITE (2,2001) GL, ORG, ELECTR
     WRITE (2,2002) (YCCF(J), J=1, MCEG1)
     GO TO 35
С
С
        CALCULATE RADILS, PRINT FINAL RESULTS.
С
   34 RADIUS = (2_{\bullet}0 + RACIUS) / (YMAX + DHG + GRAV)
     WRITE ($,3022) RACIUS
     WRITE ($,3023) (VOLTS(I),W(I),Y(I),YEST(I),ERROR(I),
    1 I=1, NPTS
С
C.
        TEST TO SEE IF LAST DATA SET.
С
   35 READ (1,1004) NDATA
     IF (NCATA) 1,36,1
   36 STOP
     END
     SUBROUTINE FITECC
С
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```
C PLRPOSE
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```
C FITS THE DATA PCINTS WITH POLYNOMIALS FROM DEGREE 3
C TO 10, FINDS THE RMS DEVIATION OF THE POINTS FROM
C EACH FITTED POLYNOMIAL AND THE 1ST AND 2ND
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```
CERIVATIVES AND THEIR ROCTS (BOTH REAL AND COMPLEX)
C
С
           FOR EACH POLYNOMIAL. THE "BEST FIT" (THE
           POLYNOMIAL OF HIGHEST DEGREE WHICH HAS NO POINT OF
С
C
C
           INFLECTION IN THE REGION OF THE CATA) IS FOUND.
C
C
         NCTE - (1) IF IER>O WHEN FINDING THE ROOTS OF THE
           SECOND DERIVATIVE OF A POLYNOMIAL (SEE SUBROUTINE
С
           POLET FOR A CEFINITION OF IER), THE GIVEN
Č
           POLYNOMIAL IS PRESUMED TO HAVE A POINT OF
С
           INFLECTION.
č
                 (2) IF ALL POLYNOMIALS HAVE A POINT OF
С
           INFLECTION IN THE REGION OF THE CATA, THEN THE
С
           POLYNCMIAL OF DEGREE 10 IS PRESUMED TO BE THE
С
           "BEST FIT".
С
С
         OTHER SUBROUTINES REQUIRED
С
           CPL SPA
С
           PDER
С
           PVAL
С
           POLRT
С
           CPXCRD
С
           PCLA
С
С
              N, X(100), Y(100), W(100), COF(11), DCOF(10),
      COMMON
              DDCOF(9), RMS, WTRMS, XMAX, YMAX, MDEG,
     1
               YEST(100), ERROR(100), CRG(5), ELECTR(5),
     2
              WTFACT(5), DATE(5), MSTART, Z
     3
      DIMENSION COF1(11), YEST1(10C), ERROR1(100), XMAX1(9),
                 YMAX1(9), XMAXR(9), XMAXI(9), XFLX(8),
     1
                 YFLX(8), XFLXR(8), XFLXI(8)
     2
                         COFD(11), CCOFC(10), DDCOFD(9),
      DOUBLE PRECISION
                         WCOF(10), RCOTR(9), ROOTI(9)
     1
      INTEGER Z
      EQUIVALENCE (XMAXR, XFLXR), (XMAXI, XFLXI)
С
С
 2001 FORMAT (/ POLYNOMIALS FIT TO DATA (VCLTS,Y) FOR 1,544/
     1 2X, 5A4, 1X, 5A4
 2002 FCRMAT (1X,5A4)
 2003 FORMAT (/// POLYNOMIAL OF DEGREE ', 12/3X,
     1 COEFFICIENTS, IN ORDER OF ASCENDING POWER OF VOLTS "/
     2 10X, "POLYNOMIAL", 11X, "1ST DERIV", 12X, "2ND DERIV")
 2004 FORMAT ( 1P3E21.7)
 2005 FORMAT (/*
                    RMS DEVIATION = +, F6.3, 9X, WEIGHTED RMS +,
     1 • DEVIATION = •, F6.3)
 2006 FORMAT (/*
                    EXTREMA*)
 2007 FORMAT (5X, "REAL ROOTS"/9X, "VCLTS", 8X, "Y-ESTIMATE")
 2008 FORMAT (F14.4.F16.3)
 2009 FORMAT (1P2E21.7/ E21.7)
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```
2010 FORMAT (5X, 'THERE ARE NO REAL ROCTS')
 2011 FORMAT (/*
                    INFLECTION POINTS")
 2012 FORMAT (/5x, 'ERROR IN POLRT SUBRCUTINE, IER =',I2)
 2028 FORMAT (5X, THERE ARE NO COMPLEX ROOTS )
 2029 FCRMAT (5X, COMPLEX ROOTS')
 2030 FORMAT ( 1PE20.6, E16.6, * * I')
 2031 FORMAT (///* ALL POLYNOMIALS HAVE POINTS OF INFLECTION*
     1 //* BEST FIT TO CATA IS ASSUMED TO BE POLYNOMIAL OF*,
     2 • DEGREE 10.•)
С
С
С
          PRINT TITLES FCR INFORMATICN TO BE FOUND
С
      WRITE (Z,2001) ORG,ELECTR,DATE
      WRITE (Z,2002) WTFACT
      TUWYLC = 0.0
      IERFIT = 1
      M = MSTART
С
С
         FIT DATA POINTS WITH LEAST SQUARES POLYNOMIAL
С
    1 CALL CPLSPA (M,N,X,Y,W, COFD,TUWYLC)
      TUWYLO = 1.0
      MP1 = M + 1
      MM2 = M - 2
      DC 6 J = 1.MP1
    6 \text{ COF1}(J) = \text{SNGL}(\text{COFD}(J))
С
С
          FIND CERIVATIVES OF POLYNOMIAL AND PRINT RESULTS
С
      CALL PDER (DCCFD, M, CCFD, MP1)
      CALL PCER (DDCOFD, MM1, DCOFD, M)
      WRITE (Z,2003) M
      WRITE (Z_{2004}) (CCFD(J), DCOFD(J), CCCOFD(J), J=1, MM1)
      WRITE (Z,2009) COFD(M), DCOFD(M), COFD(MP1)
С
C
C
         FIND Y-ESTIMATES & ERRORS FOR EACH POINT AND FIND AND
         PRINT RMS DEVIATIONS
С
      SUMW = 0.0
      SUMSQ = C_{\bullet}O
      SUMSQW = 0.0
      DC 7 I = 1, N
      CALL PVAL (YEST1(I), X(I), COF1, MP1)
      ERROR1(I) = YEST1(I) - Y(I)
      SUMW = SUMW + W(I)
      SUMSQ = SUMSQ + ERROR1(I) ** 2
      SUMSQW = SUMSQW + W(I) + ERROR1(I) + 2
    7 CONTINUE
      WTRMS1 = SORT (SUMSQW/ SUMW)
```

```
RMS1 = SQRT (SUMSQ / FLCAT(N))
      WRITE (Z,2005) RMS1, WTRMS1
С
С
          FIND THE ROOTS OF THE 1ST CERIVATIVE, PUT THE REAL
С
         ROOTS IN ORDER & FIND THEIR Y-ESTIMATES.
С
      CALL POLRT (DCOFD, WCCF, MM1, ROCTR, ROOTI, IER)
      CALL CPXCRD (MM1, FOOTR, ROOTI, NRMAX , XMAX1, NCMAX, XMAXR,
     1 XMAXI)
      DO 5 J = 1, NRMAX
    5 CALL PVAL (YMAX1(J), XMAX1(J), COF1, MP1)
С
         PRINT RESULTANT EXTREMA
С
С
      WRITE (Z,2006)
      IF (IER) 101,101,102
  102 WRITE (Z,2012) IER
  101 IF(NRMAX ) 15,15,14
   15 WRITE (2,2010)
      GO TO 103
   14 WRITE (Z,2007)
      WRITE (Z,2008) (XMAX1(J),YMAX1(J), J=1,NRMAX)
  103 IF (NCMAX) 104,104,105
  104 WRITE (Z,2028)
      GO TO 17
  105 WRITE (Z,2029)
      WRITE (Z,2030) (XMAXR(J),XMAXI(J), J=1,NCMAX)
С
         FINC THE ROOTS OF THE 2ND CERIVATIVE, PUT THE REAL
С
С
         RCOTS IN ORDER & FIND THEIR Y-ESTIMATES.
С
   17 CALL PCLRT (DDCOFC, WCOF, MM2, RCCTR, ROOTI, IER)
      CALL CPXORD (MM2, ROOTR, ROOTI, NRFLX, XFLX, NCFLX, XFLXR,
     1 XFLXI)
      DO 13 J = 1, NRFLX
   13 CALL PVAL (YFLX(J),XFLX(J),COF1,MP1)
С
         PRINT RESULTANT INFLECTION POINTS
С
С
      WRITE (Z, 2011)
      IF (IER) 106,106,107
  107 WRITE (Z, 2012) IER
  106 IF (NRFLX) 19,19,20
   19 WRITE (Z,2010)
      GC TC 16
   20 WRITE (Z,2007)
      WRITE (Z,2008) (XFLX(J),YFLX(J), J=1, ARFLX)
   16 IF (NCFLX) 108,108,109
  108 WRITE (Z,2028)
      GO TO 18
```

```
---
```

```
109 WRITE (Z,2029)
      wRITE (Z,2030) (XFLXR(J),XFLXI(J), J=1,NCFLX)
   18 IF (IER) 26,26,122
С
С
          IF NO POINTS OF INFLECTION IN REGION OF DATA, STORE
С
          YEST, ERROR, COF, DCOF, DDCOF, RMS, WTRMS.
С
   26 IF(NRFLX) 9,9,753
  753 DO 22 J = 1, NRFLX
      IF (X(1) - XFLX(J)) 21,22,22
   21 IF (XFLX(J) - X(N)) 122,22,22
   22 CONTINUE
    9 IERFIT = 0
      MDEG = M
      CALL PCLA (YEST, N, YEST1, N)
      CALL PCLA (ERROR, N, ERROR1, N)
      CALL PCLA (COF, MP1, COF1, MP1)
      DO \ 13C \ J = 1.MM1
      DCOF(J) = SNGL(DCOFD(J))
  130 DDCOF(J) = SNGL(DCCOFO(J))
      DCOF(M) = SNGL(DCCFD(M))
                                                      - -
      RMS = RMS1
      WTRMS = WTRMS1
C
C
         FIND WHICH MAXIMUM POINT IS IN THE REGION OF THE DATA
С
      DO 4 J = 1, NRMAX
      K = J
      IF (X(1) - XMAX1(J)) 8,4,4
    8 \text{ IF } (XMAX1(J) - X(N)) 10,4,4
    4 CONTINUE
      XMAX = 0.0
      YMAX = 0.0
      GO TO 122
   10 \times MAX = \times MAX1(K)
      YMAX = YMAX1(K)
  122 IF (M-10) 121,120,120
  121 M = M + 1
      GO TO 1
С
         IF ALL POLYNOMIALS HAVE POINTS OF INFLECTION, ASSUME
С
С
         THE HIGHEST DEGREE POLYNOMIAL IS THE BEST FIT.
С
  120 IF (IERFIT) 2,2,3
    3 WRITE (Z,2031)
      GO TC 9
С
    2 RETURN
      END
```

```
SUBROUTINE CPXORD (NIN, CRIN, CIIN, NROUT, RROUT, NCOUT,
     1
                            CROUT .CIOUT)
С
      DIMENSION RROUT(10), CROUT(10), CICUT(10)
      DOUBLE PRECISION CRIN(10), CIIN(10)
С
С
          SEPARATE INPUT COMPLEX NUMEERS (CRIN + CIIN * I) INTO
С
          PURE REAL NUMBERS (RROUT) AND COMPLEX NUMBERS (CROUT
С
С
          + CIOUT + I).
С
      NROUT = 0
      NCOUT = 0
      DO 1 I = 1.NIN
      IF (CIIN(I)) 2,3,2
    3 \text{ NROUT} = \text{NROUT} + 1
      RROUT(NROUT) = SNGL(CRIN(I))
      GO TC 1
    2 \text{ NCOUT} = \text{ NCOUT} + 1
      CROUT(NCOUT) = SNGL(CRIN(I))
      CIDUT(NCOUT) = SNGL(CIIN(I))
    1 CENTINUE
С
С
          PUT PURE REAL NUMBERS IN ORDER FROM SMALLEST TO
С
          LARGE ST.
С
      M = NROUT - 1
      IF (M) 4.4.5
    5 \text{ DO } 6 \text{ I} = 1, M
      K = I + 1
      DO 6 J = K, NROUT
      IF (RROUT(I) - RROUT(J)) 6,6,7
    7 X = RFOUT(I)
      RROUT(I) = RROUT(J)
      RROUT(J) = X
    6 CONTINUE
С
    4 RETURN
      END
```

C SECOND PROGRAM FOR ANALYSIS OF ELECTROCAPILLARY DATA С С С CCMMON NCONCS, NVOLTS, VSTART, VINC, MBASE, BBASE, M, B, CONC, ACT, LNACT, VOLTS, YBASE, Y, PI 1 TITLE(40), ORG(5), ELECTR(5), NAME(5), DIMENSION ABASE(11), M(10), CONC(10), A(11,10), 1 BBASE(11), LNACT(10), B(11,10), VCLTS(40), 2 YBASE(40), Y(40,10), PI(10,40), ACT(10) 3 REAL NAME, LNACT С 1001 FORMAT (20A4/20A4) 1002 FORMAT ("1 "///1X, 20A4/2X, 20A4) 1003 FORMAT (//* INPUT PARAMETERS *//4X,* ORG*, 20X, * ELECTR*, 1 17X, "NAME"/4X, 5A4, 3X, 5A4, 3X, 5A4) 1004 FORMAT (2110,4F10.0) 1005 FORMAT (/4X, "NCONCS", 4X, "NVOLTS", 4X, "VSTART", 6X, "VINC", 1 6X, "VECM", 8X, "CO") 1006 FORMAT (110,F10.C) 1 CO7 FORMAT (// INPUT COEFFICIENTS FOR POLYNOMIALS) 1008 FORMAT (1P4E15.7) 1009 FORMAT (/3X, "CONCN", 6X, "0.0", 3X, 10F10.6) 1010 FORMAT (3X, DEGREE, 18, 10110/) 1011 F CRMAT (16,3X,11F1C.2) 1012 FORMAT (// COEFFICIENTS OF TRANSFORMED PCLYNOMIALS / (NOW IN TERMS OF VOLTS VS. ELECTROCAPILLARY . 1 • 2 * MAXIMUM OF */* BASE ELECTRCLYTE) *) 1013 FORMAT (2110, 3F10.3, F10.4) С INITIALIZE ALL POLYNOMIAL COEFFICIENTS TO ZERO. С C DO 7 I=1,11 ABASE(I) = 0.0BBASE(I) = 0.0DO 7 J=1,10 A(I,J) = 0.07 B(I,J) = 0.0С С READ IN & WRITE OUT DATA C 4 READ (1,1001) TITLE WRITE (3,1002) TITLE READ (1,1001) ORG, ELECTR, NAME WRITE (3,1003) ORG, ELECTR, NAME READ (1,1004) NCONCS, NVOLTS, VSTART, VINC, VECM, CO WRITE (3,1005) WRITE (3,1013) NCCNCS, NVOLTS, VSTART, VINC, VECM, CO READ (1,1006) MBASE MP1 = MBASE + 1

READ (1,1008) (ABASE(I), I=1, MP1) DO 1 J=1,NCONCS READ (1,1006) M(J),CCNC(J) MP1 = M(J) + 11 READ (1,1008) (A(I,J),I=1,MP1) WRITE (3,1007) WRITE (3,1009) (CCNC(J), J=1, NCONCS) WRITE (3,1010) MBASE, (M(J), J=1, NCONCS) DO 5 I=1,11 K = I - 15 WRITE (3,1011) K, ABASE(I), (A(I,J), J=1, NCONCS) TRANSFORM POLYNOMIALS TO VOLTS VS. E.C.MAX. CALL SHIFT (MBASE, VECM, APASE, PBASE) DO 2 J=1, NCONCS ACT(J) = CONC(J) / COLNACT(J) = ALOG (ACT(J))2 CALL SHIFT (M(J), VECM, A(1, J), B(1, J)) WRITE (3,1012) WRITE (3,1009) (CONC(J), J=1, NCCNCS) WRITE (3,1010) MBASE, (M(J), J=1, NCONCS) 00 6 I=1,11 K = I - 16 WRITE (3,1011) K, BBASE(I), (B(I, J), J=1, NCONCS) CALL FINDPI

```
CALL COMBIN (NCONCS, NVOLTS, VOLTS, YBASE, Y, ORG, ELECTR,
1 NAME)
```

```
C
C
```

С

C C

С С

C C

С

```
READ (1,1006) NDATA
IF (NCATA) 4,3,4
3 STOP
END
```

SUBROUTINE SHIFT (M,X,A,B) C C PURPOSE C TRANSFORMS THE EQUATION OF A POLYNOMIAL WHEN THE C ORIGIN IS SHIFTED TO A NEW POSITION (X,O) ALONG THE C X-AXIS. C DESCRIPTION OF PARAMETERS

```
M = DEGREE OF POLYNOMIAL
```

108

```
X = X - VALUE (IN OLC COCRCINATE SYSTEM) OF NEW
С
С
                 ORIGIN
С
            A = ARRAY OF COEFFICIENTS OF CLD PCLYNOMIAL.
С
                 CRDERED FROM SMALLEST TO LARGEST POWER
С
            B = ARRAY OF COEFFICIENTS OF NEW POLYNOMIAL
С
С
       DIMENSION A(11), B(11)
С
       MP1 = M + 1
       B(1) = 0_{\bullet}
       DO 3 I = 1, MP1
    3 B(1) = B(1) + A(1) + X + (I-1)
С
       DO 2 J = 2, MP1
       \mathsf{JM1}=\mathsf{J}-\mathsf{1}
       B(J) = 0_{\bullet}
       DO 2 I = J,MP1
      U = 1.
       DO 1 K = 1, JM1
    1 U = U + (FLOAT(I-K) / FLOAT(K))
•
    2 B(J) = B(J) + U + A(I) + X + (I-J)
С
      RETURN
      END
      SUBROUTINE FINDPI
С
          PURPOSE
С
            FINDS VALUES OF THE INTERFACIAL TENSION (Y) AND OF
С
C
            THE SPREADING PRESSURE (PI) AS A FUNCTION OF
            POTENTIAL AND CONCENTRATICN OF ORGANIC SOLUTE AND
С
C
            PRINTS THESE VALUES IN TWO TABLES.
С
Ĉ
          OTHER SUBROUTINES REQUIRED
С
            PVAL
С
С
               NCONCS, NVOLTS, VSTART, VINC, MBASE, BBASE,
      COMMON
               M, B, CONC, ACT, LNACT, VOLTS, YBASE, Y, PI
     1
                  BBASE(11), M(10), E(11,10), CONC(10),
      DIMENSION
                  LNACT(10), VOLTS(40), YBASE(40), Y(40,10),
     1
                  PI(10,40), VL(3), ACT(10)
     2
      REAL
           LNACT
С
 1001 FCRMAT ("1"////" INTERFACIAL TENSION (Y)"//
            SOLUTION *,12X,*BASE*, 19,9110)
     1 *
                  CONCENTRATION, 13X, 10F10.6)
 1002 FORMAT (*
```

```
1003 FORMAT (* LN(C/CO)*.18X.10F10.4)
 1004 FORMAT (13X, VOLTS')
 1005 FORMAT (F18-3-11F10-2)
 1006 FORMAT ("1"////" SPREADING PRESSURE (PI)"//
     1 •
           SOLUT ION • , 5X, 10 [ 10 ]
 1007 FORMAT (*
                   CONCENTRATION, 3X, 10F10.6)
 1008 FORMAT (*
                   LN(C/CO) *,8X,10F10.4)
 1009 FORMAT (8F10.4)
 1010 FORMAT (8F10.2)
 1011 FCRMAT ('
                   ACTIVITY (C/CO), 11X, 10F1C.6)
 1C12 FORMAT ( *
                   ACTIVITY (C/CO) +,10F10.6)
 1013 FCRMAT (F6.3,2X,3A4)
С
      DATA VL/12HVOLTS VS ECM/
С
      MP1 = MBASE + 1
      DO 1 K=1, NVOLTS
      REALK = FLOAT (K-1)
      VOLTS(K) = VSTART + REALK * VINC
    1 CALL PVAL (YBASE(K), VOLTS(K), BBASE, MP1)
С
      DC 2 J=1, NCONCS
      MP1 = M(J) + 1
      DO 2 K=1.NVOLTS
      CALL PVAL (Y(K,J), VOLTS(K), B(1,J), PP1)
    2 PI(J,K) = YBASE(K) - Y(K,J)
С
      WRITE (3,1001) (J, J=1, NCONCS)
      WRITE (3,1002) (CCNC(J), J=1, NCONCS)
      WRITE (3,1011) (ACT(J), J=1,NCONCS)
      WRITE (3,1003) (LNACT(J), J=1,NCONCS)
      WRITE (3,1004)
С
      DO 3 K=1,NVOLTS
      WRITE (3,1005) VOLTS(K), YBASE(K), (Y(K,J), J=1, NCONCS)
    3 CONTINUE
С
      WRITE (3,1006) (J, J=1, NCONCS)
      WRITE (3,1007) (CONC(J), J=1, NCONCS)
      WRITE (3,1012) (ACT(J), J=1,NCONCS)
      WRITE (3,1008) (LNACT(J), J=1,NCCNCS)
      WRITE (3,1004)
С
      DO 4 K=1,NVOLTS
    4 WRITE (3,1005) VOLTS(K), (PI(J,K), J=1,NCONCS)
С
      WRITE (2,1009) (LNACT(J), J=1,NCCNCS)
      DO 5 K=1, NVOLTS
      WRITE (2,1013) VOLTS(K), VL
    5 WRITE (2,1010) (PI(J,K), J=1, NCONCS)
```

С С

RETURN

```
SUBROUTINE COMBIN (NCONCS, NVOLTS, VOLTS, YBASE, Y, ORG;
    1 ELECTR, NAME)
С
C
        PURPOSE
С
          GRAPHS ELECTRICAPILLARY CURVES FOR PURE ELECTROLINE
С
          AND FOR ALL CONCENTRATIONS OF ORGANIC SOLUTE AND THE
С
          SAME GRAPH.
С
               VOLTS(40), YBASE(40), Y(40,10), ORG(5),
     DIMENSION
               ELECTR(5), NAME(5), XL(5), YL(5), GL(5),
    1
               DL(5), LABL(7)
    2
          NAME , LABL
     REAL
С
            /20HVOLTS VS. E.C. MAX. /,
     DATA XL
             /20HGAMMA (DYNES/CM)
                                  1,
    1
         YL
                                  1,
    2
             /20H
         GL
    3
             /20H
         DL
                                  1.
         LABL/28HELECTROCAPILLARY CURVES FOR /
    4
С
     CALL ORIGIN (1.0,1.5,1)
     CALL GRAPH (NVOLTS, VOLTS, YBASE, 0, 2, 4.0, 5.5, 0.4, -0.8,
    1 20.0,320.0,XL,YL,GL,DL)
     DO 1 J=1,NCONCS
   1 CALL GRAPH (NVOLTS, VCLTS, Y(1, J), 0, 2, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0)
     1 0,0)
     1 0)
     CALL LETTER (0.0,-1.25,0.15,ELECTR,0.C,20,0,0,0,0,0,0,0,0,0
    1 0,0,0)
     1 (.0)
     CALL ORIGIN (7.0.0.0.0)
С
     RETURN
     END
```

```
C
          PREGRAM FUR FITTING FRUMKIN EQUATION TO ELECTRO-
Ċ
         CAPILLARY DATA FREM A COMPOSITE PI VS. LN ACT CURVE
Ĉ
С
      REAL #4
               CRG(5), ELECTR(5), NAME(5), LNAL(5), PIL(5),
               THL(5), REDAL(5), VL(5), FOL(5), F1L(5),
     1
               GL1(5), GL2(5), GL3(5), GL4(5),
     ź
                                           G(50), TH(50).
     3
               LNA(100), FI(100),
               x(50), Y(5G), TH$(21), LNA$(21), PI$(21),
     4
               RECA$(21), V(50), FU(50), F1(50),
     5
               LNAI, LNA2, LNAC, LNAINC, LAHAF
     6
      INTEGER CUT
                    (LNA,V), (FI,TH$,FC),
      ECUIVALENCE
                                            (LNA$,F1),
                    (G. PI$), (X. RELA$)
     1
L,
С
 1001 FCRMAT (2044)
 1002 FORMAT (IIC,F1C.0)
 1003 FERMAT (8F10.0)
 1004 FCRMAT (2F10.0)
 1005 FURMAT (2110)
C
 2CC1 FCRMAT (*1*////* FRUMKIN ECLATION FIT TO ELECTRO*,
     1 CAFILLARY DATA FUR 1/2X,5A4,1X,5A4,1X,5A4/1 ABSCISSA
     2 * CF CCMPCSITE PI VS. LN A CURVE IS *,5A4)
                 TEETA(1, 12, 1) = 1, E5.3)
 2CO2 FERMAT (/*
 2003 FORMAT (/* MAXIMUM SURF/CE_EXCESS = *,F5.3,*X10**(-10*
     i ,•) MOLES/CM++2•/• ACTIVITY FOR HALF COVERAGE = •,
     2 1PE5.3/ ALPHA = ', CPF7.4/'
                                     B - ZERG = ., 1PE9.3/
          E-ZERG-PRIME = *.CPF6.4/*
                                     ECUATION FOR ISOTHERN
     3 1
     4 "LN(TH/(A*(1-TH))) = (",F704,")*TH + (",F603,")"/
     5 • EQUATION OF STATE PI = (•, F7.3,•) +TH++2 + (•, F6.2,
     6 * )*LN(1-TH) * )
 2004 FERMAT (/
                 SURFACE +,4X, "THETA", 5X,"LN A", 6X,"LN A*, 8X,
     1 "A",6X, "A/AHALF",5X, "P1",8X, "PI"/3X, "EXCESS", 13X,
     2 •(EXPTL)•,3(3X,•(CALCD)•),3X,•(EXPTL)•,3X,•(CALCD)•)
 2015 FORMAT (F8-2, F10-3, 2F10-2, F11-4, F5-2, 2F10-1)
 2CUE FORMAT ("1"////" FREE ENERGIES OF ADSCRPTION FOR "/2X,
     1 544, 1X, 544, 1X, 544/ PETENTIAL IS IN UNITS OF , 544//

• PETENTIAL, 2X, 'LNAINC', 4X, 'LN AHALF', 3X, 'F(00)', 5X,
     2
     2 F((1))
 2007 FORMAT (2F9.3,3F10.2)
Ű
С
C
         PLT ALPFANUMERIC CATA INTO ARRAYS FOR GRAPH LABELS.
C
                  /20HFI (DYNES/CM)
                                            1,
      DATA
            FIL
                                            1,
     1
            THL
                  /20ETHETA
            RECAL /20HA/AHALF
                                            1,
     Z
     3
            FÜL
                  /20H-F(OC) (KCAL/POLE)
                                           1.
```

```
/208-F(01) (KCAL/MULE) /,
     4
             F1L
                   /20HLS FIT TO FRUNKIN EQ/,
     5
             GL 1
                   /2CHCCMPCSITE CURVE FOR /,
     6
             GL2
     7
             GL 2
                   /2GHDIMENSICALESS ISCTH./.
             GL4
                  /2CHFREE ENERGY OF ACS. /
     8
Ċ
      IN = 1
      OLT = 3
   12 READ (IN, 1001) ORG, ELECTR, NAME, LAAL
      WRITE (OUT,2001) CRG, ELECTR, NAME, LNAL
      READ (IN,1CC5) NCPT, CPT
      IF (NCPT.EC.1) GC TU 13
      READ (IN. 1004) GMAX
      GE TE 14
С
         CALCULATE GARRA-MAX FROM POINTS ON MONCLAYER PORTION
٢
Ü
         OF COMPOSITE CURVE (READ IN ACTUAL DATA POINTS).
С
   13 READ (IN.1002) N
      REAC (IN, 1CC4) (LNA(I), FI(I), I=1,N)
      CALL FOLSPA (N.LNA.PI.A.E)
      GMAX = B / 2.4789
С
С
         CALCULATE GAFRA, THETA, AND Y FROM SLOPES OF
С
         TANGENTS TO COMPOSITE CURVE (READ IN POINTS FROM
С
         HAND DRAWN TANGENTS & FROM HAND FIT TO CURVE).
С
   14 READ (IN.1002) #
      N = 1
      DC 2 I=1.M
      READ (IN, ICU3) LNAI, PI1, LNAZ, FI2, LNA(I), PI(I)
      G(N) = (FI2 - PI1) / (2.4789 + (LNA2 - LNA1))
      TE(N) = G(N) / GPAX
      IF (TH(N) - 1.0) 7.8.8
    8 WRITE (OUT,2002) I,TH(N)
      GC TC 2
    7 X(N) = ALCG (TH(N) / (1 \cdot C - TF(N)))
      Y(N) = X(N) - LNA(N)
                                      - .
      N = N + 1
    2 CONTINUE
      N = N - 1
С
         FIT LN A VS. THETA WITH FRUMKIN EQUATION.
C
С
      IF (NCPT-EC-1) GC TC S
      REAC (IN, 1004) A, E
      GC TC 10
    5 CALL FELSPA (N,TH,Y,E,A)
   10 \text{ BZERC} = \text{EXP(B)}
      ALPHA = A / 2.0
     .
```

```
D = -2.4789 * GMAX
      C = ALPHA + C
      AHALF = EXP (-1 \cdot C + (C \cdot 5 + A + B))
      EZP = AHALF * BZERC
      WRITE (CUT,2003) GMAX,AHALF,ALPHA,BZERO,EZP,A,E,C,C
C
         CALCULATE THEORETICAL LN A AND FI.
С
С
      WRITE (OUT,2004)
      DC 3 I=1,N
      LNAC = X(I) - A \neq TH(I) - B
      PIC = C \neq TH(I) \neq TH(I) + D \neq ALCG (1 \cdot 0 - TH(I))
      AC = EXP (LNAC)
      REEAC = AC / AFALF
    3 WRITE (GUT,2005) G(I),TH(I),LNA(I),LNAC,AC,REDAC,PI(I),
     1 PIC
С
         CALCULATE POINTS FOR THEORETICAL CURVES.
С
Ü
      Ths(1) = 0.025
      T_{1}(2) = 0.05
      TF_{(21)} = C_{0}975
     DC 4 1=3,20
    4 \text{ TH}(I) = \text{TH}(I-1) + C_005
     DC 5 I=1,21
     LNA$(1) = ALGG (TH$(1) / (1_0 - TF$(1))) - A * TH$(1)
     ì - B
      PI$(I) = C * TH$(I) * TH$(I) + C * ALCC (1 - C + TF$(I))
    5 \text{ REDA$(I)} = \text{EXP} (\text{LNA$(I)}) / \text{AHALF}
С
     CALL GRAFH (N,TH, LNA, 1,7,12°C, E°C, C°L, O°C, O'C, THL, LNAL,
     1 GL1,CRG)
     CALL GFAFH (21,TH$,LNA$,C,2,C,C,C,C,U,U,C,C,C,U,U)
     1 0,0)
     CALL LETTER (10.C.7.G5.C.1.NAME,G.,20,C.C.C.C.C.C.0.0,0,0,
     1 (,0)
     READ (IN,1CO3) XSIZE,XSF,XMIN,YSF,YMIN
         THESE PARAMETERS SHOLLD BE THE SAME AS FOR EC4.
C
     CALL GRAPH (21,LNA$,PI$,C,2,XSIZE,10.C,XSF,XMIN,YSF,
     1 YPIN, LNAL, PIL, GL2, CRG)
     XG = XSIZE - 2 \cdot G
     1 ()
     CALL LETTER (X0,5.65,6.1,NAME,6.,20,0,0,C,C,C,C,C,C,C,0,0,0,0
    1 ()
     IF (NCPT. EC.1) GC TU 11
     CALL GRAPH (21, RECA$, TH$, 0, 2, 10.0, 8.0, 1.0, 0.0, 0.0, 2, 0.0,
    1 REDAL, THL, GL3, ORG)
```

```
1 (,()
  1 ()
     FIND FREE ENERGIES.
  READ (IN, 1002) N.CC
  READ (IN. 1001) VE
  WRITE (CUT,2006) ORG,ELECTR,NAME,VL
  T = ALCG (AHALF)
  U1 = -1 \cdot U = (T + E + ALUG (55.5 / CO))
  U_2 = -3_0 G * (T + B + A)
  DC 6 I=1.N
  READ (IN,1003) V(I), LNAINC
  LAHAF = LNAINC + T
  F(1) = C_{0}5923 + (11 + LAHAF)
  F1(I) = C_{\bullet} 5923 * (U2 + LAHAF)
  WRITE (CUT,2007) V(I),LNAINC,LAHAF,FG(I),F1(I)
  FC(I) = -1.0 + FC(I)
c F1(I) = -1.0 + F1(1)
  CALL GRAFE (N, V, FC, 1, 11, 8.0, 1C.C, C.2, -C.E, C.4, 2.C,
 1 VL,FOL,GL4,CRG)
  1 6.01
  1 ()
  CALL GRAPH (N, V, F1, 1, 11, 8. C, 1(. (, G. 2, -G. 8, 0. 4, 0. 8,
 1 VL.F1L.GL4.LRG)
  1 0.0)
  CALL LETTER (6.0, 9.05, 0.1, NAME, C., 20, C, C, C, C, C, 0, 0, 0, 0, 0,
 1 0)
11 READ (IN, 1002) NDATA
  IF (NCATA.GT.U) GC TO 12
  STEP
  END
  SUBROLTINE FELSPA (N.X.Y.A.E)
  REAL #4
        X(1) \cdot Y(1)
         SUMX, SUMY, SUMX2, SUMXY, XD, YD, NC, BC, AD
  KEAL*8
  SUMX = U \cdot U E U
  SUMY = 0.000
  SUMXZ = C_{\bullet}CUC
  SUMXY = C.CDU
  DC 1 I=1.N
  XC = CELE(X(I))
  YC = DBLE(Y(I))
```

С С

C

C

. .

```
SUMX = SLMX + XC
SLMY = SUMY + YD
SUMX2 = SUMX2 + XD*XC
I SUMXY = SUMXY + XC*YC
NC = CFLCAT(N)
BC = (ND + SUMXY - SUMY + SUMX) / (NC + SUMX2 - SUMX + 1)
AL = (SUMY) - ED + SUMX) / NC
A = SNGL(AC)
E = SNGL(AC)
E = SNGL(ED)
RETURN
ENC
```

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APPENDIX C

Output Data From Computer Programs

- EC1 Sample of output data from program EC1. Corresponds to Figures 2-5 of Appendix A. Page 118
- EC2 The first page for each compound lists the coefficients of the polynomials fit to each electrocapillary curve by program EC1. The second page lists the interfacial tensions computed from the polynomials for various potentials and concentrations of adsorbate. Page 119
- EC5 Parameters of Frumkin equation fit to electrocapillary data for each compound. Tables of values of various surface variables. Page 127

REST FIT TO CATA FOR PUPE WEIGHTS WERE USED

C. 1001N HCL04 (7-9-58) #2

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VNDNI AL DE DECORE ID LAR DE

PCLYNOMIAL OF DEGREE IC WAS REST FIT. RMS DEVIATION = 0.622 COORDINATES OF ELFCTROCAPILLARY MAXIMUM ARE (-0.479.425.602)

• •

0.300	0.220	0.200	0.150	0.100	C. 050	0.0	-C. 050	-0.100	-0.150	-0.200	-0.250	-0,300	-0.350	-0+400	-0.450	-C.500	-0,550	-0.600	-0.650	-0.700	-C. 750	-0.800	-C.85C	-0.900	-0.950	-1.000	-1.050	-1.100	VOL TS	
0.371	0.184	06.2.0	0.397	0-1 54	0.025	0.244	0.171	0.166	0•399	0.151	0.139	0.219	0.053	0.216	0.252	0.333	0.283	0.329	0.277	C•347	0.392	0.396	0.393	0.311	0.361	0.395	0.398	966 0	WE I GHT	
348.502	216 • 154	366.767	374.929	382.512	385.377	395.779	401.463	406.660	411.185	415.177	418.472	421.257	423.277	424 762	425.458	425.551	424.948	423.694	421.814	419.424	416.546	413.204	409.445	405.314	400.744	395-802	390.444	384.761	VIEXPTL;	
348.500	357.926	366.746	374.939	382.501	389.439	395.766	401.495	406.635	411.188	415.151	418.508	421.240	423-325	424. 745	425.485	425.544	424.935	423.684	421.833	419.434	416.539	413.199	409 . 448	405.302	400.757	355.800	390.441	384.762	Y (CALCD)	
-0.002	0.014	-0-021	0.01 C	-0.010	0.063	-0.013	0.032	-0.025	E 0C*0	-0.026	0.036	-0.017	0.049	-0.017	0.026	-0.007	-0.013	-0.010	0.01 9	C •010	-0.006	-0.005	E 00°0	-0.013	0.013	-0.002	-0.003	0.001	ERROR	
19.44	18,25	17.02	15.75	14.50	13.26	12.05	10.87	09.60	8. 52	7.32	6 . 10	4.83	3, 51	2.16	0.80	-0.56	-1.87	-3+12	-4.27	-5-31	-6.25	-7.10	- 7- 90	- 8 - 69	-9, 50	-1 Ca 33	-11.09	-11.55	o	
22.81	24.33	25.11	25.27	24.98	24.46	23.92	23.52	23.41	23.64	24.19	24.98	25.87	26.67	27 . 20	27.29	26.80	25.69	24.03	21.97	19.78	17.79	16.36	15.73	15.92	16.51	16.36	13. 31	3.72	n	

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SECOND ANALYSTS OF ELECTRICATELEZAY CATA FOR 3-PENTANJE IN CALCON HOLDA - LATA CHILA + KOMPETERC

INPLT PARAMETERS

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CRG 3-PENTAN	ICL.	FLECT Tic O.	N 100N HOLC4		ME TA DE	C.	BRUACHEAD
NCONCS 7	NVÚLTS 26	VSTAR T -L.633	V INC 0+050	VECM -C.478	0.58	C.0 80	

INPUT COEFFICIENTS FOR FOLYNOWITES

CENEN	ũ.L	6.004650	C.(121eC	C.C2432C	0.046230	0.092460	C.231140	0.462280
DEGREE	16	16	10	6	S	8	9	10
ú	354. °S	394. Pi	394•Cl	354.74	393.57	398.66	388.14	382.26
1	-118.40	-112.5c	-113.ću	-115.53	-104-99	-81.37	-55.43	-41.01
Z	-104.72	-97.59	-89.18	-154.71	-149.05	-37.34	-227.65	-171.42
3	-42.37	-24.18	-74.91	24.55	92.17	136.12	-424.71	-288.90
4	-151.63	-226.74	-45C.12	87.93	-40.40	-1555.53	28.21	-52.58
5	155.48	26.65	297•26	-14.15	-649.56	-6566.57	2459.47	734.15
6	547.45	76+.56	2030.91	-41.80	-296.10	-9749.18	5885.81	914.49
7	-0. 57	362.20	578.10	C.G	E61. 89	-6531.52	6449.51	-326.49
8	-759.76	-c74.79	-3(20.06	C.0	51.87	-1665.17	3470.15	-1370.06
5	-517.66	-776.81	-3127.70	C+C	290.01	0. C	740.55	-963.84
10	-152.57	-225.92	-904.98	(•(0.0	0.0	0.0	-225.89

COEFFICIENTS OF TRANSFORMED POLYNOMIALS

INCH IN TERMS OF VOLTS VS. ELECTROCAPILLARY MAXIMUM OF BASE ELECTROLYTE)

CONCN	6.0	C. CL4650	C.C1216C	C.C2432C	0.046230	0.092460	0.231140	0.462280
CEGREE	10	10	10	£	5	8	9	10
C	425.56	424 . 72	421.38	415.5C	468.61	461.14	391.03	383.34
1	-0+07	3.26	11.53	14.34	21.68	20.90	17.90	16.93
2	-142.00	-135.01	-116.06	-81+81	-35.95	-15.88	-29+84	-30+23
3	-40.42	-75.60	-199.97	-95.59	-152.72	-128.87	-38.44	-6.67
4	136.92	103.42	56.50	- 5. 56	-199.33	-432.53	21.43	48.74
5	114.86	259.75	£75•01	100.73	355.32	239.08	172.38	-28.16
6	-297.67	-237+49	-494.06	-41.80	340.83	1452.26	-207.71	-346.33
7	-193.11	-466.15	-1714.18	C.O	-474.88	-163.91	-728.97	-96.03
8	237. 36	346.20	1123.97	C.∎C	-252.72	-1665.17	284.29	475.33
9	1C9.62	307.08	1198.07	C.O	280.01	0.0	740.55	110.92
10	-152.57	-225.94	-964.97	C.C	C • C	0.0	0 • C	-225.89

INTERFACIAL TENSION (Y)

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SCLUTICN	445 E	1	ĩ	3	4	5	£	7
CONCENTRATION		(.004850	0.012160	9.C2432G	Ŭo 0 462 30	0.052460	0.231140	0.462280
ACTIVITY (C/CC)		((8249	056320+0	J.C41361	0.078622	0.157245	C.393095	0.786190
LN(C/CU)		-4.7577	-3. 8785	-3.1854	-2.5431	-1.8500	-0.5337	-0.2406
VOLT S								
-C.033	353.20	363.12	382.77	383.42	381.29	377.67	369.84	362.63
-0.583	335.10	388664	386.28	3 8 8 • 74	395.76	381.58	372.36	365.10
-0.533	7=4.54	394.21	393.62	353.02	385.60	384.27	374.74	367.41
-C.4R3	355.54	395.20	396.58	356.56	392.86	38c.55	376.99	369.54
-0.433	434.22	463.77	402.95	355.56	395.61	389.71	375.08	371.49
-C.363	438.44	467.89	40ć•65	402+21	397.88	390.78	380.97	373.29
-ù.332	412.27	411.58	409.73	464.59	399.77	392.68	362.68	374.95
-5-253	415.64	414.65	412.30	466.79	401.36	394.37	384.23	376.50
-C.233	418.67	4 17. 7C	414.51	468.82	402.78	395.82	385.65	377.95
-0.183	421.19	420.13	416.46	410.69	404.C9	397.09	386.97	379.32
-0.133	423.19	422.10	41e.20	412.36	405. 37	398.25	388.21	380.58
-C.063	424.62	423.57	419.71	413.00	406.64	399.35	389.36	381.73
-C.(33	425.41	424.47	420.87	414.94	407.86	400.44	390.41	382.75
J.C17	425.52	424.74	421.55	415.72	408.57	401.49	391.32	383.62
C.C.7	424.91	424.31	421.EC	416.06	405.85	402.42	392.08	384.34
0• 117	423.57	423.15	420.50	415.50	410.38	403.09	392.66	384.90
C.167	421.52	421.25	415.38	415.17	410.41	403.31	393.04	385.32
0.217	41 8.77	416.61	417.01	413. 8C	409.81	402.91	393.20	385.58
Ŭ•267	415.28	415.28	413.86	411.75	40 8. 47	401.73	392.13	385.66
C•317	411.40	411+31	41C.CC	4(8,96	406.30	399.71	392.77	385.52
0.367	406.87	466.75	405.55	465.41	403.28	396.90	392.04	385.07
C•417	401.43	461.67	400.62	461.68	399.40	353.44	39C•77	384.19
C.467	396.26	356. (9	395.25	3 5 5 • 57	394.71	389.55	388.72	382.69
6.517	390.21	240.05	385.44	350.C7	399.25	385.44	385.61	38C.38
0.567	383.56	383.44	383.12	3 8 3 • 4 3	383.10	381.Ŭ8	381.12	377.05
0.617	376•35	376.28	376.16	376.06	376.27	375.98	375.08	372.49

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SECOND ANALYSIS OF ELECTRICAPILLARY DATA FOR CHLURDFORM IN C.LLCN FOLDA - DATA LA D. PROADFEAD

INFLT PARAMETERS

1

CRG Cheorcho	4 H	ELFCT IN C.	R ICTN FCLO4	NA D4	ME TA OF D.	BROADHEAD
NCONCS	NVOLTS 25	VSTAFT -C.GCG	VINC 0.050	VECM -C•474	CO 0.0454	

INFLT COEFFICIENTS FOR POLYNOMTALS

CCNCN	Ú∎l-	033510.0	C.C1782C	0.025130	0.031630	0.037690	0.044500	0.046000	C-C49400
DEGREE	10	10	10	5	9	10	10	10	10
C	395 . 10	354.50	354.80	394.54	394.19	394.22	394.19	394.40	393.82
1	-117.56	-118.0e	-116.59	-116•CC	-122.67	-118.53	-113.61	-112.70	-101.49
2	-123.57	-10(+87	-115.00	-101.73	-115+60	-132.02	-192.58	-216.85	-291.57
3	-107.06	-1.74	-34.16	7.50	210.EC	193.50	95.44	156.18	-79.29
4	162.2¢	-155.12	-41.67	-356+25	2.67	-68.21	687.99	1272.62	2003.71
5	1492 . 7u	-153.11	340.64	-5ċ1.80	-1401.64	-1718.15	338.45	773.64	3568.81
5	374.52	3 94 , üC	203.05	1244.21	-1595+40	-972.28	-2325-15	-5627.91	-5674.99
7	-7021.54	727.98	-2009.79	3451.65	791.22	4745.39	-6317.46	-15559.37	-25276.71
ε	-12969.39	225.47	-4(59.C4	2873.52	1936.93	8215.44	-7831.92	-18187.77	-32596.39
9	-9149.99	-192.19	-2965.17	818.13	750.76	5043.36	-4858.74	-10352.92	-18937-59
10	-2346.91	-115.41	-771.98	0.0	0.0	1102.92	-1194.29	-2334.60	-4167.46

CCEFFICIENTS OF TRANSFORMED POLYNOMIALS (NOW IN TERMS OF VOLTS VS. ELECTRUCAFILLARY MAXIMUM OF BASE ELECTRULYTE)

、 、

CCNCN	ŭ " C	C.C1258C	0.017820	0.025130	C.C3163C	0.C37690	0.044500	C.C450CC	0.049400
DEGREE	10	10	10	\$	9	10	10	10	10
Û	425.60	424.00	423.49	421.77	419.29	416.74	414.C¢	413.09	409.45
1	0.05	-L.c.	C•41	1.23	-0.27	-2.21	-2.26	-2.70	-3.14
ž	-147.13	-125.15	-125.67	-56.35	-54.55	- 20.65	-31.27	-33-20	-58.16
3	-89.57	-45.59	-n0 • 84	-67.14	-27.73	2.66	-21.94	- £•2C	-12.22
4	227.25	25.72	34.38	-152.21	-420.50	-509.08	-273.37	-147.68	321.20
5	599.39	157.77	242.96	311.75	52.49	-131.05	149.83	63.78	160.27
ć	-945.05	27.15	-321.48	55 C •0C	1248.31	1540.57	170.71	-554.03	-2530.91
7	-1855.66	-351.45	-735.75	-827.43	-481.18	289.97	-655.43	-494.06	-777.74
÷,	2335.69	-15.91	765.40	-016.62	-1265.83	-2148.54	820.70	2374.02	5629.99
9	1574.37	367.47	643 . 99	81 E • 1 3	750.76	-184.48	802 . 2C	713.09	916.15
10	-2346.91	-1.5.41	-771.97	G⊕ C	C•C	1102.92	-1194.29	-2334.60	-4167.45

INTERFALIAL TENSION (V)

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HASE	l	ž	3	4	5	£	7	8	
	i ∎ i 12580	0.017820	J.C2513C	0.031630	0.037690	0.04450C	0.046000	0.049400	
	(.254655	C•36C725	0.568704	0.640283	C. 762955	6.900810	0. 531174	1.000000	
	-1.3673	-1.(196	-(.6759	~0.4458	-0.2706	-0.1045	-0.0713	0.0	
357.67	387.39	367.20	367.10	387.00	386.87	386.62	386.56	386-02	
393.27	392. 82	392.58	392.39	372.24	392.14	391.80	391.71	391-09	
398+21	397.85	397.58	397.26	396.93	356.98	396.62	396-50	395.73	
492.56	462.33	402.25	401.63	401.41	401.44	401-C1	406.82	399.65	
407.41	406.82	406.51	4 66 . 06	40 5. 61	405.45	404-81	404-49	402-68	
411.44	416.69	410.32	4(9.83	409.35	408-50	407.90	407-40	404-85	
414.97	414.12	413.66	412.08	412.5C	411.70	410-24	409-57	404.35	
418.00	417•C7	416.51	415.76	414.96	413.80	411.89	411-08	407.35	
420.56	419.53	416.90	417.91	416.76	415-25	412-58	412-08	408.17	
422.64	421.45	420.83	419.55	417.99	416-14	413-63	412.69	409.77	
424.23	422.51	422.26	420.73	418.76	416.60	41 3. 97	413.02	409.22	
425.24	423.78	423-17	421.47	419-17	416.77	414-10	413-15	409.44	
425. EC	424. C6	423.49	421.77	419-29	416-74	414-06	413.09	400 45	
425.22	422.71	423-19	421-58	415-13	416-55	412-86	412.97	400 14	
424.07	422.70	422.23	420-85	418-65	416-17	413-47	412.47	407014	
422.14	421.02	426-58	419.51	41 7. 74	415.48	412-82	411.84	407 77	
419.48	416.65	416.26	417.50	416-26	414-33	411.79	410 02	406 90	
416.18	415-61	415 29	414.79	414-09	412.56	410-20	400 40	405 47	
412.33	411.52	411.70	411.37	411-11	410-00	408-16	407 72	406 39	
407-58	467-62	407-53	4(7.27	407-26	406-55	405.29	405 13	404020	
4.) - 17	462.74	402-80	402-55	402.55	402-19	403020	402012	9020 92	
357.85	367-34	367.53	357-26	397.07	304.50	204.91	307.00	397002	
191.56	351.43	351-69	361-45	396-93	301-05	370801	397.00	390.09	
395-41	385.00	385.26	365-12	384. 29	394.53	371011	391.50	140.48	
378-20	378-03	378.21	378.22	307027	277 50	20402L 277 10	309002	384.40	
	513605	JIJOEL	310022	31 10 21	511030	311+16	311.20	\$76.81	
	$\begin{array}{c} + & A \leq L \\ \hline & B \leq T = 0 \\ \hline & A \geq T = 0 \\ \hline & A =$	HASE1 G_{-25465} -1.3673 332.77 372.77 372.77 372.77 372.77 372.77 372.765 402.764 402.764 402.764 414.97 422.64 421.47 422.64 422.87 422.64 422.74 423.78 422.14 422.74 422.14 412.33 411.62 407.63 407.62 403.17 402.74 391.785 367.34 395.41 385.03 378.03	HASE12 $i \circ Cl25E0$ $0 \circ Cl7820$ $(\circ 25425)$ $-1 \circ 3673$ $-1 \circ 3673$ $-1 \circ Cl56$ $332 \circ 27$ $352 \circ 27$ $332 \circ 27$ $352 \circ 27$ $372 \circ 27$ $352 \circ 27$ $412 \circ 27$ $422 \circ 53$ $402 \circ 25$ $411 \circ 44$ $410 \circ 69$ $410 \circ 32$ $414 \circ 97$ $414 \circ 97$ $414 \circ 12$ $413 \circ 66$ $416 \circ 92$ $416 \circ 92$ $422 \circ 56$ $422 \circ 64$ $421 \circ 47$ $422 \circ 64$ $422 \circ 64$ $422 \circ 64$ $422 \circ 51$ $422 \circ 64$ $422 \circ 51$ $422 \circ 64$ $422 \circ 70$ $422 \circ 23$ $422 \circ 14$ $421 \circ 27$ $422 \circ 14$ $421 \circ 27$ $422 \circ 14$ $422 \circ 27$ $422 \circ 27$ <td>HASE123$i \circ C125FO$$0 \circ C17820$$0 \circ C2513C$$i \circ 254655$$C \circ 36C725$$0 \circ 508704$$-1 \circ 3673$$-1 \circ C156$$-C \circ 6755$$372 \circ 27$$352 \circ 27$$352 \circ 27$$372 \circ 27$$352 \circ 56$$392 \circ 58$$378 \circ 21$$357 \circ 55$$397 \circ 58$$378 \circ 21$$357 \circ 55$$397 \circ 58$$402 \circ 56$$4C2 \circ 53$$402 \circ 25$$414 \circ 42 \circ 56$$4C2 \circ 53$$414 \circ 47$$414 \circ 12$$414 \circ 77$$416 \circ 69$$412 \circ 56$$417 \circ 67$$412 \circ 56$$417 \circ 67$$416 \circ 51$$415 \circ 76$$416 \circ 69$$410 \circ 32$$416 \circ 96$$417 \circ 67$$416 \circ 56$$417 \circ 67$$416 \circ 56$$417 \circ 67$$422 \circ 64$$423 \circ 61$$422 \circ 64$$423 \circ 61$$422 \circ 64$$423 \circ 78$$423 \circ 78$$423 \circ 78$$423 \circ 76$$422 \circ 77$$425 \circ 22$$423 \circ 71$$423 \circ 17$$421 \circ 78$$424 \circ 77$$422 \circ 70$$422 \circ 23$$420 \circ 85$$422 \circ 14$$421 \circ C2$$423 \circ 15$$416 \circ 79$$412 \circ 33$$411 \circ 52$$411 \circ 79$$412 \circ 33$$411 \circ 52$$416 \circ 72 \circ 74$$422 \circ 73$$470 \circ 53$<</td> <td>HASE1234$c \cdot (125 E0)$$c \cdot (17820)$$c \cdot (2513c)$$c \cdot (36028)$$-1 \cdot 3673$$-1 \cdot (196)$$-c \cdot 6759$$-0 \cdot 6458$$37 \cdot 67$$367 \cdot 35$$387 \cdot 20$$387 \cdot 10$$387 \cdot 00$$372 \cdot 27$$392 \cdot 52$$392 \cdot 24$$397 \cdot 58$$392 \cdot 24$$398 \cdot 21$$397 \cdot 55$$397 \cdot 58$$397 \cdot 26$$396 \cdot 93$$492 \cdot 56$$4(2 \cdot 53)$$402 \cdot 25$$4(1 \cdot 61) \cdot 64$$411 \cdot 44$$416 \cdot 69$$410 \cdot 32$$409 \cdot 35$$414 \cdot 47$$414 \cdot 12$$413 \cdot 66$$412 \cdot 56$$416 \cdot 56$$417 \cdot c7$$416 \cdot 51$$415 \cdot 76$$416 \cdot 56$$417 \cdot c7$$416 \cdot 51$$415 \cdot 76$$412 \cdot 56$$412 \cdot 52$$422 \cdot 84$$421 \cdot 45$$422 \cdot 64$$421 \cdot 45$$420 \cdot 83$$419 \cdot 55$$417 \cdot 99$$424 \cdot 23$$422 \cdot 51$$422 \cdot 26$$422 \cdot 64$$421 \cdot 45$$422 \cdot 26$$420 \cdot 73$$418 \cdot 76$$422 \cdot 64$$422 \cdot 51$$422 \cdot 26$$422 \cdot 64$$421 \cdot 45$$422 \cdot 23$$422 \cdot 64$$422 \cdot 51$$422 \cdot 23$$422 \cdot 64$$421 \cdot 45$$422 \cdot 23$$422 \cdot 64$$422 \cdot 51$$422 \cdot 23$$422 \cdot 64$$421 \cdot 45$$422 \cdot 64$$421 \cdot 45$$422 \cdot 64$$422 \cdot 51$$422 \cdot 64$$421 \cdot 45$$422 \cdot 64$$421 \cdot 45$$422 \cdot 64$$422 \cdot 51$$423 \cdot 17$$423 \cdot 17$$423 \cdot 17$<td< td=""><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{c} \texttt{HASL} & \texttt{l} & \texttt{2} & \texttt{3} & \texttt{4} & \texttt{5} & \texttt{6} \\ \texttt{c} \texttt{c} \texttt{l} \texttt{l} \texttt{c} \texttt{c} \texttt{c} \texttt{c} \texttt{c} \texttt{c} \texttt{c} c$</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td></td<></td>	HASE123 $i \circ C125FO$ $0 \circ C17820$ $0 \circ C2513C$ $i \circ 254655$ $C \circ 36C725$ $0 \circ 508704$ $-1 \circ 3673$ $-1 \circ C156$ $-C \circ 6755$ $372 \circ 27$ $352 \circ 27$ $352 \circ 27$ $372 \circ 27$ $352 \circ 56$ $392 \circ 58$ $378 \circ 21$ $357 \circ 55$ $397 \circ 58$ $378 \circ 21$ $357 \circ 55$ $397 \circ 58$ $402 \circ 56$ $4C2 \circ 53$ $402 \circ 25$ $414 \circ 42 \circ 56$ $4C2 \circ 53$ $414 \circ 47$ $414 \circ 12$ $414 \circ 77$ $416 \circ 69$ $412 \circ 56$ $417 \circ 67$ $412 \circ 56$ $417 \circ 67$ $416 \circ 51$ $415 \circ 76$ $416 \circ 69$ $410 \circ 32$ $416 \circ 96$ $417 \circ 67$ $416 \circ 56$ $417 \circ 67$ $416 \circ 56$ $417 \circ 67$ $422 \circ 64$ $423 \circ 61$ $422 \circ 64$ $423 \circ 61$ $422 \circ 64$ $423 \circ 78$ $423 \circ 78$ $423 \circ 78$ $423 \circ 76$ $422 \circ 77$ $425 \circ 22$ $423 \circ 71$ $423 \circ 17$ $421 \circ 78$ $424 \circ 77$ $422 \circ 70$ $422 \circ 23$ $420 \circ 85$ $422 \circ 14$ $421 \circ C2$ $423 \circ 15$ $416 \circ 79$ $412 \circ 33$ $411 \circ 52$ $411 \circ 79$ $412 \circ 33$ $411 \circ 52$ $411 \circ 79$ $412 \circ 33$ $411 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SECOND ANALYSIS OF ELFORNCOAPILLARY DATA FOR CYCLOHERANDE IN LOLON HELDA - FATA LE F. BREACHEAD ICONCEC/COL

INPUT PARAMETERS

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CRG CYCLOHEX	ANGL	ELECT. In C.	105N HOLC4	N4 C4	AME ATA CF D.	BRUPDHEAD
NCUNCS	RVULTS	VSTAFT	VINC	VEC₩	CC	
6	25	-6.600	0.050	-℃•479	1.0000	

INPUT COEFFICIENTS FOR POLYNOMIALS

CENCN	u∎G	C.0250C0	L.C5CCCC		0.225000	C.450000	6.900000
DEGREE	16	9	Ş	10	10	10	10
C	355.77	395.32	395.12	393.53	389.22	3 82 • 84	374.35
1	-120+51	-118.72	-112.32	-94.31	-59.18	- 36.26	-40.30
ž	-119.58	-126.08	-203.96	-277.91	-278.35	-198.31	-206+33
3	-16.49	98.51	225.54	SC+23	-347.77	-433.23	-281.42
4	-26.36	-371.71	706.23	1412.5C	£54 . 26	-174.24	556.4C
5	1C5.CO	-954.19	- 755 • 72	679.18	2816.58	1461.Cl	1978.80
6	120.24	1264.54	-4685.73	-5706.84	263.08	32 84. 89	-259.77
7	-12].95	4526.31	-5135.50	-12232.21	-8173.93	2738.28	-7538.20
a	-129.32	3855.16	-2824.87	-10645.27	-12650.88	508.44	-11566.28
ÿ	44 . El	1062.64	-525.31	-4282.OC	-7845.83	-516.83	-7309.87
10	45.71	-105.41	-771.58	-636.71	-1012.40	-223.90	-1731.15

CCEFFICIENTS OF TRANSFORMED POLYNOMIALS INCW IN TERMS OF VELTS VS. ELECTRICAPILLARY MAXIMUM OF BASE ELECTROLYTE)

CCNCN	ũ.C	C. C25000	000363.0	0.10000	0,225000	C. 45CCG0	c°la00000
DEGRES	10	5	ç	10	1 10	10	10
G	425.60	416.71	468.37	399.95	390 - 54	362.09	373.66
1	-C. (5	15.87	17.51	14.52	16.94	17.76	17.86
2	-135.39	-42.00	-21.63	-21.50	-32.31	-25.74	-29.13
3	-17.85	-172.91	-39.76	64.69	1.32	-9.16	-7.46
4	102.EC	-358.89	-245.50	-20.25	167.70	46.76	131.50
5	-26.77	647.01	-254.13	-714.77	11.57	79.36	103.12
6	-207.7e	366.04	369.09	-583.40	-1209.51	-334.13	-944.73
7	138.22	-1315.04	£54.E3	1588.66	-599.03	-526.14	-764.04
8	151.54	-366.09	-361.60	1246.57	2459 . 8C	424.74	2072.72
9	-175.11	1082.64	-585.31	-1232.19	E35.54	555.67	982.34
10	45.91	-105.41	-771.57	-636•7C	-1812.39	-223,90	-1731-15

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INTERPACIAL TENSILY (V)

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STEUTIEN	15.50	ı	ĩ	ż	4	5	e
CENCENTRATION		+ + 6 25 6 63	6.05 CC C C	0.10000L	0.225000	C.450000	0.90000
ACTIVITY (C/CC)		1.425000	ü+≎5CCCC	0.100000	0.225000	3.4500CC	000000
LNIC/CO)		-3.6n8)	-2.9957	-2.3026	-1.4917	-0. 7985	-0.1054
VCLTS						-	
-Lacus	237.17	3+6.37	384.78	360.19	771.61	363.36	254-65
-6.550	392.74	351.49	369.08	342.47	37 3. 82	365-54	357.04
-C.50 C	3+7.73	395.Ll	392.39	365.40	375.95	367.61	355-07
-1.450	402.71	466.27	355.07	367.54	376.01	369.59	361.05
-6.465	-37.05	463. 27	397.33	365.44	379.92	371.44	362.54
-0.350	411+D7	4G6.E5	355.30	391.17	331.65	373.17	364.49
-C.3U0	-14.60	409.22	461.Ce	1 52 . 81	333.23	374.77	366.28
-0.250	417.31	411.CE	462.63	354.36	334.68	376-25	367.74
-0.2(3	421.50	412.53	464.64	395.91	336-05	377.62	365.11
-C.150	422.60	413.75	405.29	357.10	397.34	379.90	370-40
-C.100	424.23	414.63	466.42	358.22	238.54	380-07	371.60
-0.059	425.27	415.23	407.44	359.16	335.61	381,14	372.69
C. C	425. tu	41c.71	406.37	359.95	320.54	382-09	373.66
0.050	425.24	417.37	409-19	466.63	391. 31	382.52	374.49
C. 100	424.23	417.67	409.84	401.24	391.93	383.61	375.16
C.15C	422.53	417.42	416.24	4(1.79	29 2. 43	384-17	375.72
	420.17	416.45	410.24	462.23	392. 64	384-62	376.18
C.25C	417.17	414.71	465.67	4 62 . 43	372.15	384.94	376.55
C. 30 C	41 3.55	412.01	404.24	402-19	393.29	385.11	376-80
L.350	437.35	468.40	466.67	4C1.22	397.11	385-06	376.80
6.400	404.55	463.53	402.72	3 5 5 . 25	372.35	384-67	376-40
C.450	399.10	398.70	398.23	356.03	390.71	383.74	375, 25
C.500	353.18	392.82	352.65	351.43	397.85	381.99	273-41
4.559	386.60	386.35	386.14	365.50	383-51	379.11	370.36
C.ELC	379.40	379.31	378.93	378.50	377.62	374.80	366.12

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SECCND ANALYSIS OF ELECTROCAPILLARY DATA FUP CYCLOHEXANONE IN 0.100N HOLO4 - DATA OF D. BPCADEEAD (CONC=C/CO)

INFUT PARAMETERS

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ORG		ELECTI	R	NA	BROADHEAD	
Cyclofexanone		In 0.1	100n HCLC4	DA		
NCONCS	NVOLTS 25	VSTART -0.60C	V INC 0. C50	VEC# -0.482	C0 1• 000C	

IN PUT COEFFICIENTS FCR PCLYNOMIALS

C JNCN	0.0	0. C50000	0.237500	0.475000	0.950000
DEGREE	10	9	10	10	10
C	395.95	393.93	386.01	375.84	371.73
1	-120.74	-103.94	-60.67	-49.94	-49.12
Z	-120.73	-200-86	- 226. 25	-156.21	-201.88
3	-6.83	127.11	-188.57	-191.80	-204.93
4	-30.40	411.94	490.29	253.74	335.53
5	-22.87	-580.06	1 230. 71	826.85	1086.96
6	-75.30	-2008.19	- 603 • 44	-175.38	-254.74
7	-146.98	-1729.57	-4889.87	-2732.52	-4012.52
8	-19.54	-497.66	-6515.90	-3712.72	-5786.48
9	96. 56	-2.08	-3733.21	-2101.46	-3498.56
10	45.60	0.0	- 812.84	-446.80	- 798. 82

COEFFICIENTS OF TRANSFORMED POLYNOMIALS (NOW IN TERMS OF VOLTS VS. ELECTROCAPILLARY MAXIMUM OF BASE ELECTRCLYTE)

CONCN	0.0	0.050000	0.237500	0.4750CC	0.950000
DEGREE	10	9	10	10	10
0	425.60	403.16	385.94	378.13	369.86
1	0.03	29.85	32.09	33.23	32.55
2	-130.26	-30.57	-47.41	-45.11	-44.27
3	-12.86	-51.69	-10.51	-9.73	-11.65
4	66+ 92	-283.11	64.78	43.91	56.63
5	- 39. 26	-103.96	-80.25	-77.61	-22.21
é	-101.63	609.60	- 588. 76	-404.75	- 50 3. 63
7	126.53	172.03	-65.30	11.84	-226.45
8	36. 57	-488.65	1180.91	732.26	1038.98
9	-122-82	-2.08	184.66	52.13	351.74
10	45+60	0.0	-812.84	-446.8C	-798.82

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INTERFACIAL TENSION (Y)

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SCLUTION	BASE	1	2	3	4	5	6
CONCENTRATION		0.025000	0.050000	0.100000	0.237500	0.475000	0-950000
ACTIVITY (C/CO)		0.025000	0.050000	0.100000	0.237500	9-475000	0.950000
LN(C/CO)		-3.6889	-2. 9957	- 2- 3026	-1-4376	-0.7444	-0.0513
VOLTS							
-C. 600	387.03		372.25		353.94	345-64	337.89
-C.550	392.66		375.60		357.34	349-13	341-37
-0, 500	397.88		378.89		360.68	352.53	344.70
-0.450	402.70		382.16		36 2.92	355,80	347.01
-0.400	407.12		385.35		367-01	358.91	350.00
-0.350	411.15		388.39		369-94	361.86	25 2. 01
-C. 300	414.76		391.19		372.71	364-66	256.67
-0-250	417.92		393.73		375.33	367.32	350 74
-0.200	42 C. 60		356-00		377.81	340 93	341 74
-0.150	422-74		398-04		396.13	272 10	3010/4
-C.10C	424-31		399.90		397.29	374.27	364 10
-0-050	425.28		401-60		394. 22	276 26	340 13
C. 0	425-60		403-16		396 04	270 12	200012
0-050	425.27		404.57		307 43	370 49	30 7. 80
0-100	424.20		405.74		201042	21900	271.27
0-150	422.44		404.44		300 60	381.00	3/2.00
0-200	420-38		407.05		309000	382.00	313.13
C-250	417.47	410.43	404 85		390.90	202092	3/4.30
0.300	413 64	4.00 75	400.00		390.09	282.48	375.13
0.350	400.70	404 54	403 60	200.24	390.99	583.70	375.38
0.04.0	405 64	4000 54	403070	334.20	390.00	583.49	375.23
0.450	300 40	402040	901-05	357.00	389.58	382.73	374.53
0.400	377807	397021	397.03	394.03	357.72	381.24	373.11
	372014	371037	372.00	384.82	384.94	378.87	37C.78
0.550	387.18	384.77	385.99	384.45	380.79	375.48	367.40
G. 60C	18 Ce 00	511.53	379+16	378.12	375.51	370.96	362.88

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FRUMEIN EQUATION FIT TO ELECTROCAPILLARY CATA FOR 3-PENTANOL IN G-100N FOLO4 CATA OF D- BROADFEAD ABSCISSA OF COMPOSITE FI VS- LN & CURVE IS LN & (--0000 VS-E000)

MAXIMUM SURFACE EXCESS = 4.470X1(+4(-1G) MLLES/CM++2 ACTIVITY FCR HALF (CVERAGE = 1.650E-02 ALPHA = 1.3364 B-ZERD = 1.555E C1 P-ZERD-PRIFE = C.262H EGUATION FUR ISOTHERM LN(TH/(A+(1-TH))) = (2.6728)+TF + (2.744) EQUATION OF STATE FI = (-14.808)+TF++2 + (-11.08)+LN(1-TH)

SURFACE	THETA	LN A	LN A	. 🛕	A/AHAL F	PI	F1
EXCESS		(EXPTL)	(CALCD)	(CALCE)	(CALCO)	(EXPTL)	ICALCO)
G.51	C.115	-5.00	-5.1C	C. (C61	0.36	C.7	1.2
0.66	6.148	-4.50	-4.89	0.0075	C. 45	0.8	1.5
C.91	0.263	-4.80	-4.65	0.095	0.56	1.0	1-9
1.12	0.250	-4.70	-4.51	C.C11C	0.65	1.3	2.3
1.32	0.295	- 4. EO	-4.4C	0. C122	0.72	1.6	2.6
1.50	G.336	-4.50	-4.32	C. (133	0.78	2.0	2.9
1.77	C. 396	- 4. 40	-4.22	0.0146	0.87	2.4	3, 3
1.93	0.433	-4.30	-4.17	0.C154	0.91	2.8	3.5
2.10	0.465	-4-20	-4-12	0.C162	0.96	3-3	3.8
2.26	0, 50 5	-4.10	-4.C7	0.0170	1.01	3.8	4-0
2.51	0.563	-4. CO	-4.CO	0.0184	1.09	4.5	4.5
2.72	G.607	- 3. 50	-3.93	G. C196	1.16	5.1	4.9
2.98	0.666	-3.80	-3.63	0. (216	1.28	5.8	5.6
3.14	0.703	-3.7C	-3.76	0.6233	1.30	6.6	6.1
3.34	C. 74 E	- 3. 60	-3.66	C. C25 9	1.53	7.3	7.0
3.47	0.775	-3.50	-3.58	0.C279	1.65	8.2	7.6
3.62	ü. 810	- 3.40	-3.46	C. (315	1.86	9.1	8.7
3.77	0.843	- 3. 30	-3.32	0.0363	2.15	10.0	10.0
3.90	0.871	- 3 - 20	-3,16	0.0424	2.51	11.0	11.5
4.00	C.895	-3.10	-2.99	C. (5C2	2.57	12.0	13.1
4.07	C.910	- 3.00	-2.86	U. C570	3.37	13.0	14.4
4.12	C.921	- 2. BO	-2.75	C.C637	3.77	15.0	15.5
4.20	J. 939	- 2. 60	-2.53	C. C80C	4.73	17.0	17.9
4.25	0.951	- 2. 40	-2.33	0.0977	5.78	19-1	20.0
4.29	C. 961	-2.20	-2,12	0.1203	7.12	21.3	22.2
4.38	C. 950	- 2. 00	-1.48	0.2277	13.47	23.5	29.0

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FRUMKIN EQUATION FIT TO ELECTROPARTLLARY DATA FOR OHLOROFORM IN COLUNE HOL(4 LATA OF DO BROADFEND ABSCISSA OF COMPOSITE FILVSOLIN A CURVE IS UN ACT (C.V. VSO FOM)

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MAXIMUM SURFACE EXCESS = 7.5CGX1L**(-10) #CLES/CP##2 ACTIVITY FCP HALF CCVEHAGE = 4.4492E-01 ALPHA = 1.6552 B-ZERU = 3.345E-01 B-ZERU-FRIME = C.15C3 ECLATICA FCR ISUTHERN LN(TH/(A*(1-TH))) = (3.7904)*TH + (-1.095) EQUATICA CF STATE PI = (-35.235)*TH**2 + (-18.59)*LN(1-TH)

SURFACE	T⊢E T A	LN A	LN A	4	A /AMAL F	PI	PI
EXCESS		(EXPTL)	(CALCD)	(CALCD)	(CALCD)	(EXPTL)	(CALCD)
C+32	6.043	- 2. 40	-2.17	0,1142	C. 25	0.5	0.8
C. 36	C.048	-2.26	-2.08	0.1252	0.28	0.5	0.8
0.42	0.057	-2.00	-1.53	0.1442	C.32	C. 8	1.0
Ú. 48	C. C64	-1.90	-1.83	C.16C2	0.36	1.1	1.1
C+53	0.071	-1. tu	-1.75	0.1746	6.39	1.3	1.2
6.55	C. C7 3	-1.52	-1.72	0.1787	0.40	1.4	1.2
Uo 54	C.085	-1.44	-1. EÜ	0.2016	C. 45	1.6	1.4
0.74	C. C99	-1. 36	-1.49	0.2262	0. 50	1.7	1.6
0.30	C.107	-1.32	-1.43	0.2388	C. 53	1.8	1.7
0.51	0.121	- 1. 28	-1.35	C. 2601	0. 58	1.8	1.9
1.00	C.134	-1.24	-1.28	0.2780	C. 62	2.0	2.0
1.22	0.163	-1.20	-1.16	0.3137	0.70	2.1	2.4
1.39	C.185	-1.16	- 1. CS	C. 3366	6.75	2.2	2.6
1.58	0.210	-1.12	-1.C3	0.3587	C.80	2.3	2.8
1.71	C.228	-1.08	-6.55	C. 3715	C. 83	2.5	3.0
1.89	C.252	-1.04	-C.95	0.3876	C. 86	2.7	3.2
2.07	0.275	-1.00	-6.52	0.4005	0.89	2.9	3.3
2 . 34	ü . 31 3	- (. 56	-0.98	C.4156	C. 93	3.1	3.5
2.68	0.357	-0.92	-C.85	0.4290	0.95	3.4	3.7
3.03	C.4C3	-C.88	-0.83	C.4381	C• 98	3.6	3.9
3.38	C.450	-0.84	-C. 81	G. 4443	0.59	4.0	4.0
3.64	C.465	-C. 80	-0. EU	C.4478	1.00	4.3	4.0
3.90	0.521	-C.76	-C. 80	0.4512	1.CG	4.7	4.1
4.26	C. 56 8	-C.72	-0.78	0.4565	1.02	5.1	4.2
4.53	0.664	-C.68	-C+77	0.4620	1. (3	5.5	4.4
5.03	J.673	-0.64	-C. 73	0.4818	1.07	6.0	4.9
5.56	J. 74 2	-0•40	-C.66	0.5162	1.15	6.5	5.8
5.90	0.785	-0.56	-C. 58	0.5582	1.24	7.1	6.9
6. 2ù	C.826	- C. 52	-C• 48	C. 6159	1.38	7.7	8.5
6.36	0 . 848	-C.48	-C.4C	0• £7C 1	1.49	8.4	9.7

				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.5	0.6	6 0	L. 2	1.3	1 = 5	1.7	1.9	2.3	2.5	2.7	0.0	3.2	3.6	3.9	4.3	4 • B	5.5	6.9	8.4	5 ° 7	11.3	13.7	16.8	19.6	21.5
F &) F C 4)	Z o 744)		L T T T T	0-2	0	0.6	0.7	0.8	1.0	1.1	1.3	1.5	1.8	2.1	2.5	2.5	3.4	4 °C	4 • 6	5.4	6.1	7.0	8.0	0° 0	10.0	11.1	12.2	14.6	17. C	19•3
0. RP1.A0- 10 V VS.	**2 971#TH + () = [N(]-T+) • . • u • · E		0-17	C. 20	0.24	C. 34	C. 41	C. 46	C. 53	0.58	0.64	0.73	0.78	0. 63	0.88	0.53	0. 58	1. C4	1.10	1.17	1.28	1.48	1.71	1.94	2.24	2.79	3.67	4.64	5° 44
EATA FCF Cata CF Is Ln ACT) MCLES/CM	+ (-12•35	ICALCOL	0. EC22	0.026	0.0031	C. (C44	U. CU54	C. CC6C	0. COE 5	0. 0016	C. CC83	0. 0096	C• C1Q2	C• C1C8	0.C115	0.0121	0• C129	0.C136	0• C 1 4 4	0.C152	0.0167	c•C193	0.0224	C. C254	0• C253	C. C364	C. C475	0.0606	C.C71C
СС #Р1 L L # M N - PC L C 4 L N - A C UR V E	CX1C++(-1C 1+3C6E-G2 1A+(1-TH})	7611415462 1 8 8		-6.11	-5.55	-5.77	-5.42	-5.22	-5.12	-4.58	-4.66	-4.79	-4.65	-4.58	-4.53	-4.47	-4.42	-4.35	-4.29	-4.24	-4. 18	-4. C9	- 3• 95	-3•80	-3.67	-3•53	-3.31	- 3.0 5.4	-2 . 8C	-2.65
TC ELECTRI IN 5.1301 Tè PI VS. 1	ESS = 5.00 CVERAGE = 30 30 RP I N(TH/	PI = [-19.	(TL J	-6.00	-5.80	-5.66	- 5. 40	- 5, 30	-5.20	- 5, 10	-5.00	-4.50	- 4. 80	-4.70	-4.60	-4.50	-4.40	-4.30	-4.20	-4.10	-4.00	-3.90	- 3. 80	-3.70	-3•60	-3.50	- 3. 40	-3.20	- 3• 00	- 2. 80
UATION FLT Not UF COMPLSI	UFFACE EXC FCK HALF C 1.55543 1.5555 01 1.5555 01 1.6555 01 FCH 150745	LF SIAIE Theta		0.033	C	0. 05 5	C• C6 2	G. 105	0.120	C. 145	0.163	C.154	U. 245	C.28C	C.314	C. 359	014 0	C.4E1	C. 553	0.000	0.661	C. 720	C. 766	0 • 831	0.853	C. 554	0.912	0.936	0.951	Ce 55 \$
FRUMKIN EN CVCL JMEXA ABSC ISSA	42X[4UM 5] 4CT[V[TY] 4LPHA = B-2ERU = B-2ERU = ECLAT[CN]	SUBEACE	EXCESS	C.15	0.22	C+27	C. 41	0.53	C •60	C. 72	C.84	16.0	1.23	1.40	1.57	1.80	2.05	2. 40	2.077	3.04	3.31	3. 60	3.93	4.16	4.30	4.42	4 • 56	4.68	4.76	6. B0

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FRUNKIN EGUATIGN FIT TO ELECTROCAPILLARY DATA FOR CYCLOMERANONE IN U-100N FOLO4 DATA OF D- BRUADHEAD ABSOISSA UF COMPOSITE PI VS- EN A CURVE IS EN A (-0-7V VS- SCE)

MAXIMUM SURFACE EXCESS = 4.660X1C++(-1û) MCLES/C++2 ACTIVITY FCR HALF (DVERAGE = 5.518E-03 ALPFA = 0.5737 B-2ERC = 9.520E 01 E-2ERC-FRIME = C.5634 EQUATION FCR ISCTHERM LN(TF/(A+(1-TH))) = (1.1475)+TF + (4.556) EQUATION CF STATE PI = (-6.626)+TF++2 + (-11.55)+LN(1-TH)

SURFACE	THETA	LN A	LN A	٨	A/AHAL F	PI	PI
EXCESS		(EXPTL)	(CALCD)	(CALCE)	(CALCO)	(EXPTL)	(CALCO)
0.59	0.126	-7.00	-6.63	C. C013	C. 22	9.0	1.5
0.62	J.133	-6.80	-6.59	0.0014	0.23	1.1	1.5
0.69	0.148	-6.60	-6.48	0.0015	0.26	1.4	1.7
0.77	G.165	-6.40	-6.37	0.0017	0.29	1.8	1.9
C.80	0.172	- ۥ 20	-t. 32	0.018	0.30	2.1	2.0
0.84	C.181	-6.10	-6.27	0.0019	0.32	2.3	2.1
0.95	0.204	-6.CO	-6.15	0.0021	0.36	2.6	2.4
1.04	C. 224	- 5. 90	- ć .0ć	C. ((23	· · 0• 40	2.9	2.6
1.12	0.241	-5.80	-5.98	0. CO2 5	C+43	3.1	2.8
1.10	0.254	-5.70	-5.53	C. (C27	0.45	3.4	3.0
1.37	0.293	-5.60	-5.77	0.031	C. 53	3.7	3.4
1.59	0.340	-5,50	-5.61	0.0037	0.ť2	4.0	4.0
1.88	C.4G3	-5+40	-5.41	6.(645	0.75	4.5	4.9
2.25	0.482	- 5. 30	-5.18	0.CO56	C. 55	5.0	6.1
2.46	0.528	-5.20	-5.05	C. CC64	1.08	5.7	6.8
2.65	G. 568	- 5.10	-4. 54	0.CG72	1.21	6.2	7.6
2.93	0.628	-5.00	-4.75	0.0086	1.46	7.0	8.8
3.06	C. 656	-4.90	-4.66	0.0094	1.59	7.8	9.5
3.11	0.668	- 4. 80	-4.62	0.098	1.66	8.5	9.8
3.19	0.684	-4.70	-4.57	0.0104	1.76	9.2	10.2
3.22	0.692	-4.60	-4.54	G.C107	1. 80	10.0	10.4
3.30	C•708	~4.50	-4.48	0.0113	1.91	10.9	10.9
3.41	0.731	-4.40	-4.40	0.0123	2.08	11.8	11.6
3.51	C.754	- 4. 30	-4.3C	C. (135	2. 29	12.6	12.4
3.60	0.774	-4.20	-4.22	0.0148	2.50	13.5	13.2
3.69	0.793	-4.00	-4.12	C. C162	2.73	15.3	14.0
3.90	0.828	-3.80	-3. 53	0.0196	3.31	17.2	15.8
3.99	0.856	-3.60	-3.76	0.0234	3.55	19.1	17.5
4.09	C.878	~ 3. 40	-3.59	0•C277	4.67	21.1	19.2
4.21	0.903	- 3. 20	-3.36	0.C347	5.86	23.2	21.5
4.26	0.914	-3.00	- 3. 24	C.C392	6.62	25.3	22.8
4.34	C.931	- 2. 80	-3. (2	0.0487	8.23	27.4	25.1
4.40	0.944	-2.60	-2. 82	0.0596	10. C8	29.7	27.3
4.48	J.961	-2.40	-2.46	0.0852	14.40	31.9	31.3
4.55	0.975	- ž. 20	-1.55	C. 136C	22.99	34.0	36.5
4.59	0.985	-2. CC	-1.50	0.2235	37.84	36.3	42.1

APPENDIX D

Tables Cited in Text

Table 1	Precision of the electrocapillary curves	Page 1	32
Table 2	Orientation of molecules	Page 1	33

Adsorbate (activity)	Maximum Correction Applied for Evaporation (dynes/cm)	RMS Deviation (dynes/cm)	Percentage of Points with Error > 0.1 dyne/cm
<u>3-Pentanol</u>			
0 0.008 0.021 0.041 0.079 0.157 0.393 0.786	 	0.16 0.25 0.34 0.45 0.62 1.63 0.84 0.75	31 56 66 94 78 75 67 64
Chloroform			
0 0.225 0.361 0.509 0.640 0.763 0.901 0.931 1.000	0.13 0.13 0.40 0.36 0.56 1.03 0.88 0.72	0.18 0.14 0.10 0.14 0.24 0.17 0.22 0.25 0.27	30 20 28 42 43 35 40 48 59
Cyclohexanol			
0 0.025 0.050 0.100 0.225 0.450 0.900	0.76 0.71 0.25 0.07	0.02 0.12 0.22 0.14 0.09 0.04 0.06	0 34 48 55 17 3 7
Cyclohexanone			
0 0.025 0.050 0.100 0.238 0.475 0.950	 	0.03 0.06 0.15 0.02 0.05 0.05 0.03	0 5 60 7 7 0

Table 1.	Precision	of	the	electrocapillary	curves
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Configuration	$\Gamma_{\rm m} \times 10^{10}$ (mole/cm ²)	Area/molecule (A ²) (experimental)	Area/molecule (^{A2}) (calculated)
	7.50	22.1	19.3
Parallel	4.47	37.1	3 5
axial OH	5.00	33.2	20
equatorial OH	5.00	33.2	30
parallel	4.66	35.6	26
	Configuration Parallel axial OH equatorial OH parallel	Configuration $\Gamma_m \times 10^{10}$ (mole/cm2)7.50Parallel4.47axial OH5.00equatorial OH5.00parallel4.66	Configuration $\Gamma_{m} \times 10^{10}$ (mole/cm2)Area/molecule (\Re^{2}) (experimental)7.5022.1Parallel4.4737.1axial OH5.0033.2equatorial OH5.0033.2parallel4.6635.6

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Table 2. Orientation of molecules